# DEPARTMENT OF COMMUNITY DEVELOPMENT BUILDING, PLANNING & ON-SITE SANITATION SECTIONS



1510 – B Third Street Tillamook, Oregon 97141 www.tillamook.or.us (503) 842-3408

Land of Cheese, Trees and Ocean Breeze

# Floodway Development Permit #851-23-000136-PLNG: DAVIS

NOTICE TO MORTGAGEE, LIENHOLDER, VENDOR OR SELLER: ORS 215 REQUIRES THAT IF YOU RECEIVE THIS NOTICE, IT MUST BE PROMPTLY FORWARDED TO THE PURCHASER

# NOTICE OF ADMINISTRATIVE REVIEW Date of Notice: July 31, 2023

Notice is hereby given that the Tillamook County Department of Community Development is considering the following:

**851-23-000136-PLNG:** A review of a Floodway Development Permit for the placement of deck addition to an existing single-family dwelling near the Nehalem River. The subject property is accessed from McDonald Road, a County road, and is designated as Tax Lot 1400, of Section 24CB of Township 3 North, Range 10 West of the Willamette Meridian, Tillamook County, Oregon. The property is located in the Rural Residential 2-Acre (RR-2) Zone. The applicant and property owners are Trent and Kellie Davis.

Written comments received by the Department of Community Development prior to 4:00p.m. on August 14, 2023, will be considered in rendering a decision. Comments should address the criteria upon which the Department must base its decision. A decision will be rendered no sooner than the next business day, August 15, 2023.

Notice of the application, a map of the subject area, and the applicable criteria are being mailed to all property owners within 250 feet of the exterior boundaries of the subject parcel for which an application has been made and other appropriate agencies at least 14 days prior to this Department rendering a decision on the request.

A copy of the application, along with a map of the request area and the applicable criteria for review are available for inspection on the Tillamook County Department of Community Development website: <a href="https://www.co.tillamook.or.us/commdev/landuseapps">https://www.co.tillamook.or.us/commdev/landuseapps</a> and is also available for inspection at the Department of Community Development office located at 1510-B Third Street, Tillamook, Oregon 97141.

If you have any questions about this application, please call the Department of Community Development at 503-842-3408 Ext. 3301 or mjenck@co.tillamook.or.us

Sincerely.

Melissa Jenck, CFM, Senior Planner

Sarah Absher, CFM, Director

Enc. Applicable Ordinance Criteria, Maps

# **REVIEW CRITERIA**

# ARTICLE III – ZONE REGULATIONS

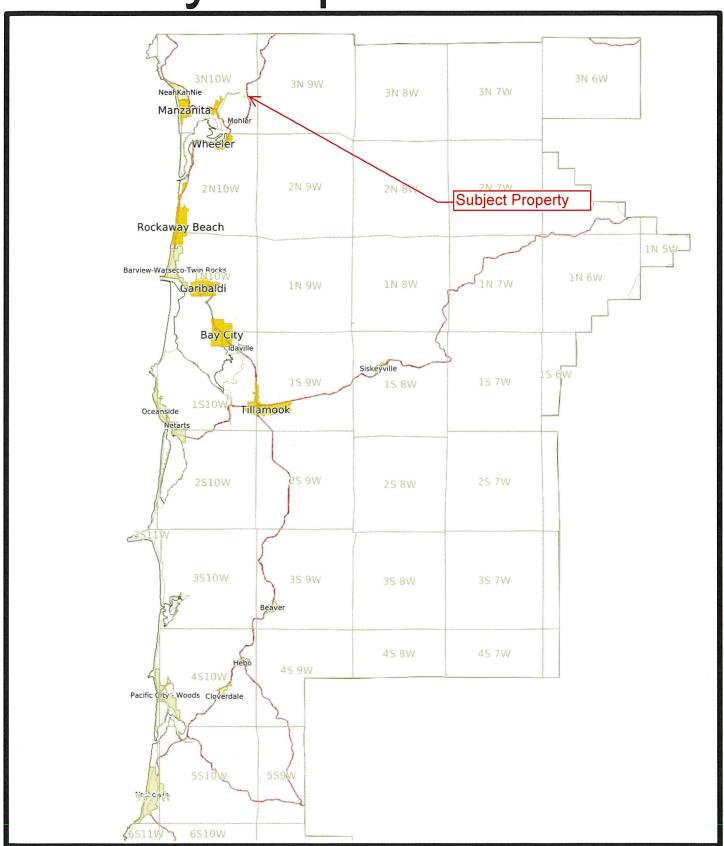
## TCLUO SECTION 3.510: FLOOD HAZARD OVERLAY ZONE

- (1) The fill is not within a Coastal High Hazard Area.
- (2) Fill placed within the Regulatory Floodway shall not result in any increase in flood levels during the occurrence of the base flood discharge.
- (3) The fill is necessary for an approved use on the property.
- (4) The fill is the minimum amount necessary to achieve the approved use.
- (5) No feasible alternative upland locations exist on the property.
- (6) The fill does not impede or alter drainage or the flow of floodwaters.
- (7) If the proposal is for a new critical facility, no feasible alternative site is available.
- (8) For creation of new, and modification of, Flood Refuge Platforms, the following apply, in addition to (14)(a)(1-4) and (b)(1-5):
  - i. The fill is not within a floodway, wetland, riparian area or other sensitive area regulated by the Tillamook County Land Use Ordinance.
  - ii. The property is actively used for livestock and/or farm purposes,
  - iii. Maximum platform size = 10 sq ft of platform surface per acre of pasture in use, or 30 sq ft per animal, with a 10-ft wide buffer around the outside of the platform,
  - iv. Platform surface shall be at least 1 ft above base flood elevation,
  - v. Slope of fill shall be no steeper than 1.5 horizontal to 1 vertical,
  - vi. Slope shall be constructed and/or fenced in a manner so as to prevent and avoid erosion.

Conditions of approval may require that if the fill is found to not meet criterion (5), the fill shall be removed or, where reasonable and practical, appropriate mitigation measures shall be required of the property owner. Such measures shall be verified by a certified engineer or hydrologist that the mitigation measures will not result in a net rise in floodwaters and be in coordination with applicable state, federal and local agencies, including the Oregon Department of Fish and Wildlife.

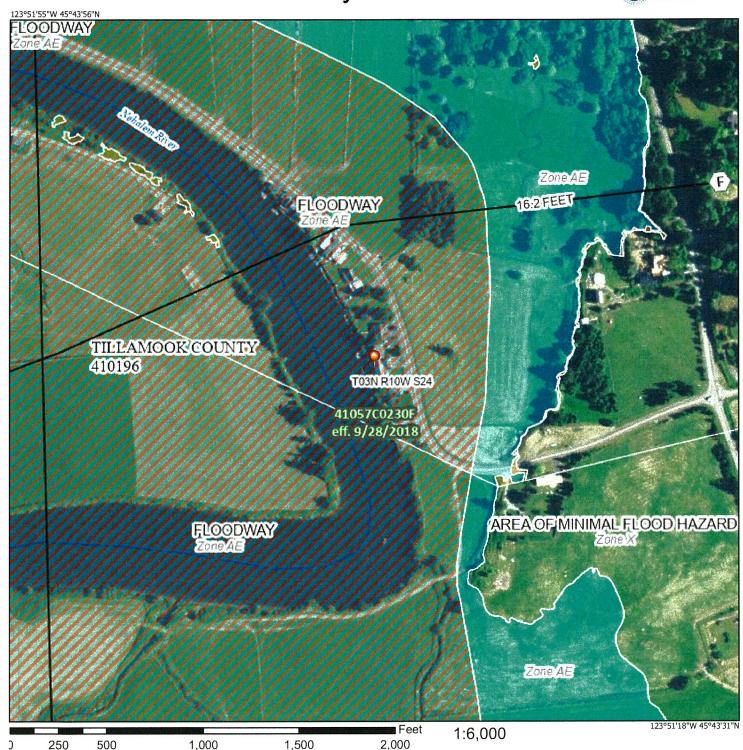
# EXHIBIT A

# Vicinity Map



# National Flood Hazard Layer FIRMette





# Legend

MAP PANELS

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

Without Base Flood Elevation (BFE) With BFE or Depth Zone AE, AO. AH. VE, AR SPECIAL FLOOD Regulatory Floodway HAZARD AREAS 0.2% Annual Chance Flood Hazard, Area of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone > **Future Conditions 1% Annual** Chance Flood Hazard Zone X Area with Reduced Flood Risk due to Levee. See Notes. Zone X OTHER AREAS OF FLOOD HAZARD Area with Flood Risk due to Levee Zone D NO SCREEN Area of Minimal Flood Hazard Zone X Effective LOMRs OTHER AREAS Area of Undetermined Flood Hazard Zone - - - Channel, Culvert, or Storm Sewer STRUCTURES | LILLIL Levee, Dike, or Floodwall 20.2 Cross Sections with 1% Annual Chance 17.5 Water Surface Elevation Coastal Transect ---- 513 --- Base Flood Elevation Line (BFE) Limit of Study Jurisdiction Boundary --- Coastal Transect Baseline OTHER Profile Baseline **FEATURES** Hydrographic Feature Digital Data Available No Digital Data Available

The pin displayed on the map is an approximate point selected by the user and does not represe an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

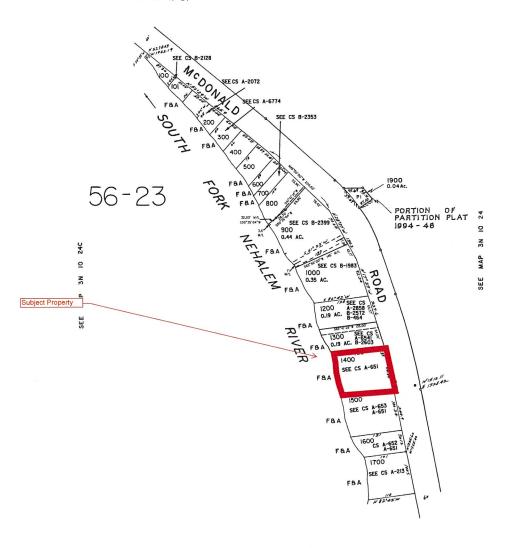
Unmapped

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 7/29/2023 at 8:29 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

CANCELLED NO. 102 1100 1800

SEE MAP 3N 10 24

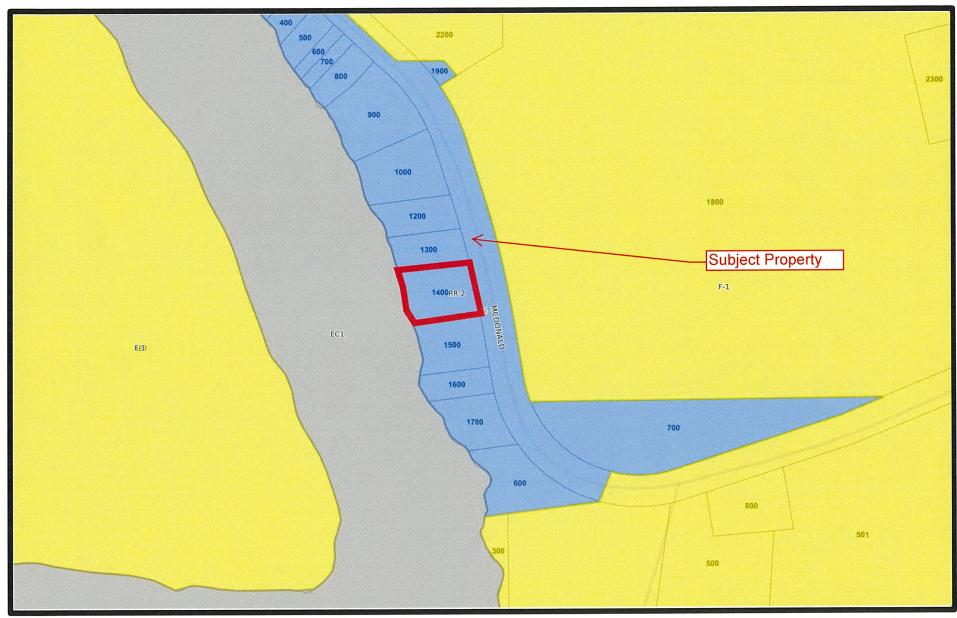


SEE MAP 3N 10 24 3N 10 24CB

REVISED 04/10/03, SA

# Zoning Map





Generated with the GeoMOOSE Printing Utilities

# **Tillamook County** 2022 Real Property Assessment Report

Account 89175

Мар

3N1024CB01400

Code - Tax ID

5623 - 89175

**Tax Status** 

Assessable

**Account Status** 

Active

Subtype

**NORMAL** 

**Legal Descr** 

See Record

Mailing

DAVIS, TRENT D & KELLIE M

13975 SW HIGH TOR DR

TIGARD OR 97224-1598

Deed Reference # 2020-2592

Sales Date/Price

04-27-2020 / \$0

**Appraiser** 

WHITNEY HOPKES

**Property Class** 

101

MA

SA

NH

**RMV Class** 101 02 WF 263

Site Situs Address	City
1 16395 MC DONALD RD	COUNTY

			Value Summary			
Code Ar	ea	RMV	MAV	AV	RMV Exception	CPR %
5623	Land	71,880		Land	0	
	lmpr	385,530		Impr	0	
Code	Area Total	457,410	216,670	216,670	0	
G	rand Total	457,410	216,670	216,670	0	

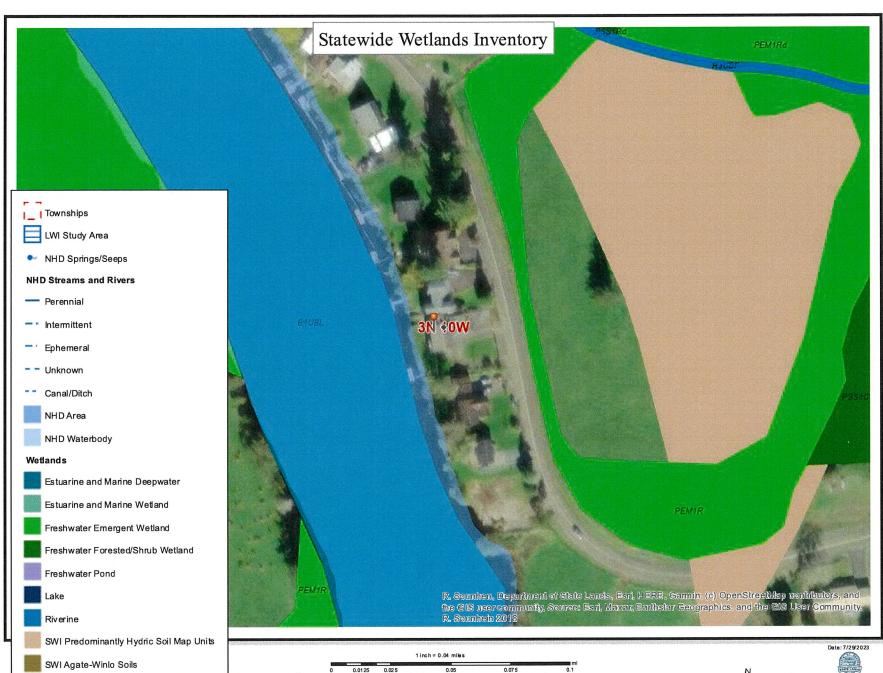
				Land I	Breakdown			
Code Area	ID#	מבמם	Plan	Walana O a sa sa	Trend			
	# טו	KFPU	Ex Zone	Value Source	%	Size	Land Class	Trended RMV
5623				LANDSCAPE - FAIR	100	·		500
	1	V	RR-2	Market	110	0.29 AC		58,880
				OSD - AVERAGE	100			12,500
ļ				Cod	le Area Total	0.29 AC		71,880

Improvement Breakdown								
Code Area	ID#		Stat Class	Description	Trend %	Total Soft	Ex% MS Acct	Trended RMV
5623	1	1967	139	Basement First Floor	169	1,286		385,530
					Code Area Total	1,286		385,530

Exemptions / Special Assessments / Notations					
Code Area 5623					
Special Assessments	Amount	Year Used			
■ SOLID WASTE	12.00	2022			

Comments

02/02/09 Updated inventory after phase one mapping.ef 1/23/15 Reappraised land and tabled values. WH



The Statewide Wetlands Inventory (SWI) represents the best data available at the time this map was published and is updated as

new data becomes available. In all cases, actual field conditions determine the presence, absence and boundaries of wetlands and waters (such as creeks and ponds). An onsite investigation by a wetland professional can verify actual field conditions.

# EXHIBIT B



Tillamook County Department of Community Development

1510-B Third Street. Tillamook, OR 97141 | Tel: 503-842-3408 Fax: 503-842-1819

www.co.tillamook.or.us

OFFICE USE ONLY

Date Stamp

# **DEVELOPMENT PERMIT**

				TO SO THE PERSON OF	
Applicant ☐ (Check Box i	f Same as Property Own	er)		MAY O A	2023
Name: Trent Day	15 Phone: 1037	200	275/	MAI U 2	7070
Address: 13975 Sta	High ton Dr	60	77) 6	BY: COU	inter
City: to and	State: on	Zip:	97774		
Email: trent Gt	D-advisors.com		67001	Approved	
	2 0000000000000000000000000000000000000			Received by:	70
Property Owner				Receipt #:	( (D)
Name:	Phone:			Fees: \(\(\cappa\) O	6.00
Address:					/ DINC
City:	State:	Zip:		851- <u>23</u> - <u>000/3</u>	-PLNG
Email:					
<b>Description of Work:</b>	You delle aden	vd.	1		
)					
Location:	1				
Site Address: 1639 C	mesocald				
Map Number:					
Township	Range		Section	on Tax L	ot(s)
Complete all applicable f	ields:		Flood Insurance	Rate Man (FIRI	M) Panel Info
	stuary: Floodplain:		Tillamook County	Panel Number: 4:	
New: Addition: Replacen		1	Effective Date: 4/28		
Dwelling:	Accessory Structure: 747		Floodway: (Y) N		
Culvert Diameter:	Bridge Length:	59.44	Stream/Waterbody		20110(3).
Length:	Width:		Neh	Slem Riv	ev
Fence Height:	Retaining Wall Height:		Elevation Data (		
Streambank Stabilization:	Other:		Base Flood Elevation		oitable Floor:
Fill/Removal/Grading: NOCY	Vegetation Removal:	CY	Lowest Floor/Horizo	1-1 -	
			Enclosed Area:	Flood Ve	ent Area:
Structure/Damage \$: 7 0 K	E Voor Construction C.			D	
- SALES CONTINUED AND THE REAL PROPERTY OF THE PERSON OF T			Other Required	Permits	
Substantial improvement/dan	nage threshold 50% cost vs. valu	ue			
Authorization					
This permit application does n	ot assure permit approval. Th	he appl	icant and/or property	v owner shall be re	sponsible for
obtaining any other necessary					
complete, accurate, and consi					
	<del>)</del>				
Property Owner Signature (Required)					Date
A I'm a A C'anada					D-1-
Applicant Signature					Date
Development Permit App	lication Rev	v. 7/15	5/21		Page 1
Perciopinent i ciniit App	HOGEROTI /ICI	//	/	1000	1 020 T

# TLCUO SECTION 3.510(14)(b) Development Permit Review Criteria:

- (1) The fill is not within a Coastal High Hazard Area.
- (2) Fill placed within the Regulatory Floodway shall not result in any increase in flood levels during the occurrence of the base flood discharge. No per No Rise propud by las lad
- (3) The fill is necessary for an approved use on the property. (C5 receded extra strays due to Flood plane strays due to (4) The fill is the minimum amount necessary to achieve the approved use. (5) No feasible alternative upland locations exist on the property. extra post on Flood plane (6) The fill does not impede or alter drainage or the flow of floodwaters.

- (6) The fill does not impede or alter drainage or the flow of floodwaters.
- (7) If the proposal is for a new critical facility, no feasible alternative site is available.
- (8) For creation of new, and modification of, Flood Refuge Platforms, the following apply, in addition to (14)(a)(1-4) and (b)(1-5):
  - i. The fill is not within a floodway, wetland, riparian area or other sensitive area regulated by the Tillamook County Land Use Ordinance.
  - ii. The property is actively used for livestock and/or farm purposes,
  - iii. Maximum platform size = 10 sq ft of platform surface per acre of pasture in use, or 30 sq ft per animal, with a 10-ft wide buffer around the outside of the platform,
  - iv. Platform surface shall be at least 1 ft above base flood elevation,
  - v. Slope of fill shall be no steeper than 1.5 horizontal to 1 vertical,
  - vi. Slope shall be constructed and/or fenced in a manner so as to prevent and avoid erosion.

Conditions of approval may require that if the fill is found to not meet criterion (5), the fill shall be removed or, where reasonable and practical, appropriate mitigation measures shall be required of the property owner. Such measures shall be verified by a certified engineer or hydrologist that the mitigation measures will not result in a net rise in floodwaters and be in coordination with applicable state, federal and local agencies, including the Oregon Department of Fish and Wildlife.



NATIONAL FLOOD INSURANCE PROGRAM

# **ELEVATION CERTIFICATE**

AND

**INSTRUCTIONS** 

**2019 EDITION** 

OMB No. 1660-0008 Expiration Date: November 30, 2022

# U.S. DEPARTMENT OF HOMELAND SECURITY Federal Emergency Management Agency National Flood Insurance Program

### ELEVATION CERTIFICATE AND INSTRUCTIONS

### Paperwork Reduction Act Notice

Public reporting burden for this data collection is estimated to average 3.75 hours per response. The burden estimate includes the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and submitting this form. You are not required to respond to this collection of information unless a valid OMB control number is displayed on this form. Send comments regarding the accuracy of the burden estimate and any suggestions for reducing the burden to: Information Collections Management, Department of Homeland Security, Federal Emergency Management Agency, 500 C Street SW, Washington, DC 20742, Paperwork Reduction Project (1660-0008). NOTE: Do not send your completed form to this address.

# **Privacy Act Statement**

Authority: Title 44 CFR § 61.7 and 61.8.

**Principal Purpose(s):** This information is being collected for the primary purpose of estimating the risk premium rates necessary to provide flood insurance for new or substantially improved structures in designated Special Flood Hazard Areas.

Routine Use(s): The information on this form may be disclosed as generally permitted under 5 U.S.C. § 552a(b) of the Privacy Act of 1974, as amended. This includes using this information as necessary and authorized by the routine uses published in DHS/FEMA-003 – National Flood Insurance Program Files System or Records Notice 73 Fed. Reg. 77747 (December 19, 2008); DHS/FEMA/NFJP/LOMA-1 – National Flood Insurance Program (NFJP) Letter of Map Amendment (LOMA) System of Records Notice 71 Fed. Reg. 7990 (February 15, 2006); and upon written request, written consent, by agreement, or as required by law.

**Disclosure:** The disclosure of information on this form is voluntary; however, failure to provide the information requested may result in the inability to obtain flood insurance through the National Flood Insurance Program or the applicant may be subject to higher premium rates for flood insurance. Information will only be released as permitted by law.

## **Purpose of the Elevation Certificate**

The Elevation Certificate is an important administrative tool of the National Flood Insurance Program (NFIP). It is to be used to provide elevation information necessary to ensure compliance with community floodplain management ordinances, to determine the proper insurance premium rate, and to support a request for a Letter of Map Amendment (LOMA) or Letter of Map Revision based on fill (LOMR-F).

The Elevation Certificate is required in order to properly rate Post-FIRM buildings, which are buildings constructed after publication of the Flood Insurance Rate Map (FIRM), located in flood insurance Zones A1–A30, AE, AH, A (with BFE), VE, V1–V30, V (with BFE), AR, AR/A, AR/AE, AR/A1–A30, AR/AH, and AR/AO. The Elevation Certificate is not required for Pre-FIRM buildings unless the building is being rated under the optional Post-FIRM flood insurance rules.

As part of the agreement for making flood insurance available in a community, the NFIP requires the community to adopt floodplain management regulations that specify minimum requirements for reducing flood losses. One such requirement is for the community to obtain the elevation of the lowest floor (including basement) of all new and substantially improved buildings, and maintain a record of such information. The Elevation Certificate provides a way for a community to document compliance with the community's floodplain management ordinance.

Use of this certificate does not provide a waiver of the flood insurance purchase requirement. Only a LOMA or LOMR-F from the Federal Emergency Management Agency (FEMA) can amend the FIRM and remove the Federal mandate for a lending institution to require the purchase of flood insurance. However, the lending institution has the option of requiring flood insurance even if a LOMA/LOMR-F has been issued by FEMA. The Elevation Certificate may be used to support a LOMA or LOMR-F request. Lowest floor and lowest adjacent grade elevations certified by a surveyor or engineer will be required if the certificate is used to support a LOMA or LOMR-F request. A LOMA or LOMR-F request must be submitted with either a completed FEMA MT-EZ or MT-1 package, whichever is appropriate.

This certificate is used only to certify building elevations. A separate certificate is required for floodproofing. Under the NFIP, non-residential buildings can be floodproofed up to or above the Base Flood Elevation (BFE). A floodproofed building is a building that has been designed and constructed to be watertight (substantially impermeable to floodwaters) below the BFE. Floodproofing of residential buildings is not permitted under the NFIP unless FEMA has granted the community an exception for residential floodproofed basements. The community must adopt standards for design and construction of floodproofed basements before FEMA will grant a basement exception. For both floodproofed non-residential buildings and residential floodproofed basements in communities that have been granted an exception by FEMA, a floodproofing certificate is required.

Additional guidance can be found in FEMA Publication 467–1, Floodplain Management Bulletin: Elevation Certificate, available on FEMA's website at <a href="https://www.fema.gov/media-library/assets/documents/3539?id=1727">https://www.fema.gov/media-library/assets/documents/3539?id=1727</a>.

# U.S. DEPARTMENT OF HOMELAND SECURITY Federal Emergency Management Agency National Flood Insurance Program

OMB No. 1660-0008 Expiration Date: November 30, 2022

# **ELEVATION CERTIFICATE**

Important: Follow the instructions on pages 1-9.

Copy all pages of this Elevation Certificate and all attachments for (1) community official, (2) insurance agent/company, and (3) building owner.

SECTION A - PROPERTY INFORMATION	FOR INSURANCE COMPANY USE						
A1. Building Owner's Name Trent D. & Kellie M. Davis		Policy Number:					
A2. Building Street Address (including Apt., Unit, Suite, and/or Bldg. No.) or Box No.	Company NAIC Number:						
16395 McDonald Road		ZID Code					
City State Nehalem Oregon		ZIP Code 97131					
A3. Property Description (Lot and Block Numbers, Tax Parcel Number, Leg 3N 10 24 CB Tax Lot 1400	A3. Property Description (Lot and Block Numbers, Tax Parcel Number, Legal Description, etc.) 3N 10 24 CB Tax Lot 1400						
A4. Building Use (e.g., Residential, Non-Residential, Addition, Accessory, e	tc.) Accessory						
A5. Latitude/Longitude: Lat. N45.72881 Long. W123.86006	Horizontal Datum	n: NAD 1927 X NAD 1983					
A6. Attach at least 2 photographs of the building if the Certificate is being u	sed to obtain flood insura	ance.					
A7. Building Diagram Number7		, and the second se					
A8. For a building with a crawlspace or enclosure(s):							
a) Square footage of crawlspace or enclosure(s)	717.00 sq.ft						
b) Number of permanent flood openings in the crawlspace or enclosure	(s) within 1.0 foot above	adjacent grade 12					
c) Total net area of flood openings in A8.b sq in							
d) Engineered flood openings?							
A9. For a building with an attached garage:							
a) Square footage of attached garagesq ft							
b) Number of permanent flood openings in the attached garage within	.0 foot above adjacent g	rade					
c) Total net area of flood openings in A9.b sq	in						
d) Engineered flood openings?							
	HAD (FIDE) INFORMA	TION					
SECTION B – FLOOD INSURANCE RATE	· · · · · · · · · · · · · · · · · · ·	B3. State					
B1. NFIP Community Name & Community Number Tillamook County, Oregon 410196A Tillamook	vame	Oregon					
B4. Map/Panel B5. Suffix B6. FIRM Index Date B7. FIRM Panel Effective/ Revised Date	B8. Flood B9. E Zone(s)	Base Flood Elevation(s) Zone AO, use Base Flood Depth)					
41057C0230F 09-28-2018 09-28-2018							
B10. Indicate the source of the Base Flood Elevation (BFE) data or base flood depth entered in Item B9:    FIS Profile   FIRM   Community Determined   Other/Source:							
B11. Indicate elevation datum used for BFE in Item B9: NGVD 1929 X NAVD 1988 Other/Source:							
B12. Is the building located in a Coastal Barrier Resources System (CBRS) area or Otherwise Protected Area (OPA)? 🔲 Yes 🗵 No							
Designation Date:							

# **ELEVATION CERTIFICATE**

IMPORTANT: In these spaces, copy the corresponding	FOR INSURANCE COMPANY USE				
Building Street Address (including Apt., Unit, Suite, and/o 16395 McDonald Road	r Bldg. No.) or P.O. Ro	ute and Box No.	Policy Number:		
City Sta Nehalem Ore		Code 131	Company NAIC Number		
SECTION C – BUILDING EL	EVATION INFORMA	TION (SURVEY RI	EQUIRED)		
<ul> <li>C1. Building elevations are based on:  Construction Drawings*  Building Under Construction*  Finished Construction *A new Elevation Certificate will be required when construction of the building is complete.</li> <li>C2. Elevations – Zones A1–A30, AE, AH, A (with BFE), VE, V1–V30, V (with BFE), AR, AR/A, AR/AE, AR/A1–A30, AR/AH, AR/AO. Complete Items C2.a–h below according to the building diagram specified in Item A7. In Puerto Rico only, enter meters.</li> <li>Benchmark Utilized: P 711  Vertical Datum: NAVD 1988</li> <li>Indicate elevation datum used for the elevations in items a) through h) below.</li> </ul>					
□ NGVD 1929 ☒ NAVD 1988 ☐ Other/	. =	<b>***</b>			
Datum used for building elevations must be the san		BFE.	Check the measurement used.		
a) Top of bottom floor (including basement, crawls	pace, or enclosure floo	r)	12.2 X feet  meters		
b) Top of the next higher floor			23.7 X feet meters		
c) Bottom of the lowest horizontal structural memb	er (V Zones only)		feet		
d) Attached garage (top of slab)			feet meters		
<ul> <li>e) Lowest elevation of machinery or equipment ser (Describe type of equipment and location in Cor</li> </ul>	vicing the building nments)		23.7 X feet meters		
f) Lowest adjacent (finished) grade next to building	g (LAG)		12.0 X feet  meters		
g) Highest adjacent (finished) grade next to buildin	g (HAG)	<del></del>	12.1 X feet  meters		
<ul> <li>h) Lowest adjacent grade at lowest elevation of de structural support</li> </ul>	ck or stairs, including		12.1 🗵 feet 🗌 meters		
SECTION D - SURVEYOR	, ENGINEER, OR AF	CHITECT CERTIFI	CATION		
This certification is to be signed and sealed by a land su I certify that the information on this Certificate represent statement may be punishable by fine or imprisonment up	s my best efforts to into	erpret the data availa	law to certify elevation information. ble. I understand that any false		
Were latitude and longitude in Section A provided by a li	censed land surveyor	Yes No	Check here if attachments.		
Certifier's Name Erick M. White	License Number PLS 78572				
Title Survey Manager			Gross R		
Company Name			GATTER ST. AND		
Onion Peak Design					
Address 11460 Evergreen Way			Here		
City Nehalem	State Oregon	ZIP Code 97131			
Signature	Date 02-21-2023	Telephone (503) 440-4403	Ext.		
Copy all pages of this Elevation Certificate and all attachments for (1) community official; (2) insurance agent/company, and (3) building owner.					
Comments (including type of equipment and location, per C2(e), if applicable)  The top of bottom floor is the concrete slab on the first floor. This area is garage/storage. The next higher floor will be the first finished floor. The lowest machinery servicing the building will be the heating located on the first finished floor.					

# **ELEVATION CERTIFICATE**

IMPORTANT: In these spaces, copy the corresponding	FOR INSURANCE O	OMPANY USE			
Building Street Address (including Apt., Unit, Suite, and/or 16395 McDonald Road	Bldg. No.) or P.O. Route an	d Box No.	Policy Number:		
CityStatNehalemOre			Company NAIC Num	ber	
SECTION E – BUILDING ELEV FOR ZONE A	ATION INFORMATION (SI O AND ZONE A (WITHOU		REQUIRED)		
For Zones AO and A (without BFE), complete Items E1–E4 complete Sections A, B,and C. For Items E1–E4, use naturenter meters.					
<ul><li>E1. Provide elevation information for the following and check the appropriate boxes to show whether the elevation is above or below the highest adjacent grade (HAG) and the lowest adjacent grade (LAG).</li><li>a) Top of bottom floor (including basement,</li></ul>					
b) Top of bottom floor (including basement, crawlspace, or enclosure) is	-	eetmeter			
E2. For Building Diagrams 6–9 with permanent flood oper the next higher floor (elevation C2.b in	<del>_</del>	<del></del>			
the diagrams) of the building is	f	eet [] mete	rs above or b	elow the HAG.	
E3. Attached garage (top of slab) is	f	eet  mete	rs above or b	elow the HAG.	
E4. Top of platform of machinery and/or equipment servicing the building is	fe	et 🗌 meter	rs above or b	elow the HAG.	
E5. Zone AO only: If no flood depth number is available, is floodplain management ordinance?   Yes No					
SECTION F - PROPERTY OWNER	R (OR OWNER'S REPRESE	NTATIVE) C	ERTIFICATION		
The property owner or owner's authorized representative v community-issued BFE) or Zone AO must sign here. The s	vho completes Sections A, B statements in Sections A, B,	and E for Zo and E are cor	one A (without a FEMA rect to the best of my l	-issued or knowledge.	
Property Owner or Owner's Authorized Representative's N	ame		· · · · · · · · · · · · · · · · · · ·	······	
Address	City	St	ate Z	IP Code	
Signature	Date	Te	elephone		
Comments				,	
			Check here it	attachments.	

# **ELEVATION CERTIFICATE**

IMPORTANT: In these spaces, copy the corre		FOR INSURANCE COMPANY USE				
Building Street Address (including Apt., Unit, Su 16395 McDonald Road	iite, and/or Bldg. No.) or F	P.O. Route and Box No.	Policy Number:			
City Nehalem	State Oregon	ZIP Code 97131	Company NAIC Number			
SECTIO	N G - COMMUNITY INF	ORMATION (OPTIONAL)				
The local official who is authorized by law or ordinance to administer the community's floodplain management ordinance can complete Sections A, B, C (or E), and G of this Elevation Certificate. Complete the applicable item(s) and sign below. Check the measurement used in Items G8–G10. In Puerto Rico only, enter meters.						
G1. The information in Section C was take engineer, or architect who is authorized data in the Comments area below.)						
G2. A community official completed Section or Zone AO.	on E for a building located	d in Zone A (without a FEM	A-issued or community-issued BFE)			
G3. The following information (Items G4–0	310) is provided for comr	munity floodplain managem	ent purposes.			
G4. Permit Number	G5. Date Permit Issued		Date Certificate of Compliance/Occupancy Issued			
G7. This permit has been issued for:	New Construction  Solution	ubstantial Improvement				
G8. Elevation of as-built lowest floor (including of the building:	basement)	feet	meters Datum			
G9. BFE or (in Zone AO) depth of flooding at the	he building site:	feet	meters Datum			
G10. Community's design flood elevation:			meters Datum			
Local Official's Name		Title				
Community Name	1	Telephone				
Signature	, C	Date				
Comments (including type of equipment and local	ation, per C2(e), if applica	able)				
			Check here if attachments.			

# **BUILDING PHOTOGRAPHS**

See Instructions for Item A6.

**ELEVATION CERTIFICATE** 

IMPORTANT: In these spaces, copy the correspon	iding information	on from Section A.	FOR INSURANCE COMPANY USE
Building Street Address (including Apt., Unit, Suite, at 16395 McDonald Road	nd/or Bldg. No.)	or P.O. Route and Box No.	Policy Number:
	State	ZIP Code	Company NAIC Number
City			Company NAIC Number
Nehalem	Oregon	97131	
If using the Elevation Certificate to obtain NFIP instructions for Item A6. Identify all photographs with "Left Side View." When applicable, photographs movents, as indicated in Section A8. If submitting more	h date taken; "Fr nust show the fo	ont View" and "Rear View"; an oundation with representative	d, if required, "Right Side View" and examples of the flood openings or
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Photo One Caption			Clear Photo One
			:
	Photo	Two	
Photo Two Caption			Clear Photo Two

**BUILDING PHOTOGRAPHS** 

**ELEVATION CERTIFICATE** 

Continuation Page

IMPORTANT: In these spaces, copy the correspon	FOR INSURANCE COMPANY USE		
Building Street Address (including Apt., Unit, Suite, a 16395 McDonald Road	nd/or Bldg. No.) or P.O		Policy Number:
City Nehalem	State Oregon	ZIP Code 97131	Company NAIC Number
If submitting more photographs than will fit on the with: date taken; "Front View" and "Rear View"; photographs must show the foundation with represe	and, if required, "Ri	ght Side View" and "L	eft Side View." When applicable,
	Photo:Three:		
Photo Three Caption			Clear Photo Three
	Photo Fou	<b>"</b>	
Photo Four Conting	Photo:Four		Clear Photo Four
Photo Four Caption			Clear Photo Four

HEAISTONS 20f East Cypress Gerbaldin OR 9118 503-322-2442 Shickerengineering.cor prineeringneering









10 - GOVER PHEE COT II - STEP FAJO SLO- BEG FCUNDANION PLAN SLO- 3-BO FOOD BEEF RANGED FLAN SLO- 2-BO FOOD BEEF RANGED FLAN SLO- WELL AND BOWN HOUSE SEAVED BAS SLO- WELL AND BOWN HOUSE SEAVED BAS SLO- WELL AND BOWN HOUSE SEAVED BAS

SHEET INDEX:

NAILING SCHEDULE

# NAILING SCHEDULE NOTES

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	- 1	
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GENERAL NOTES

STRUCTURAL DESIGN NOTES

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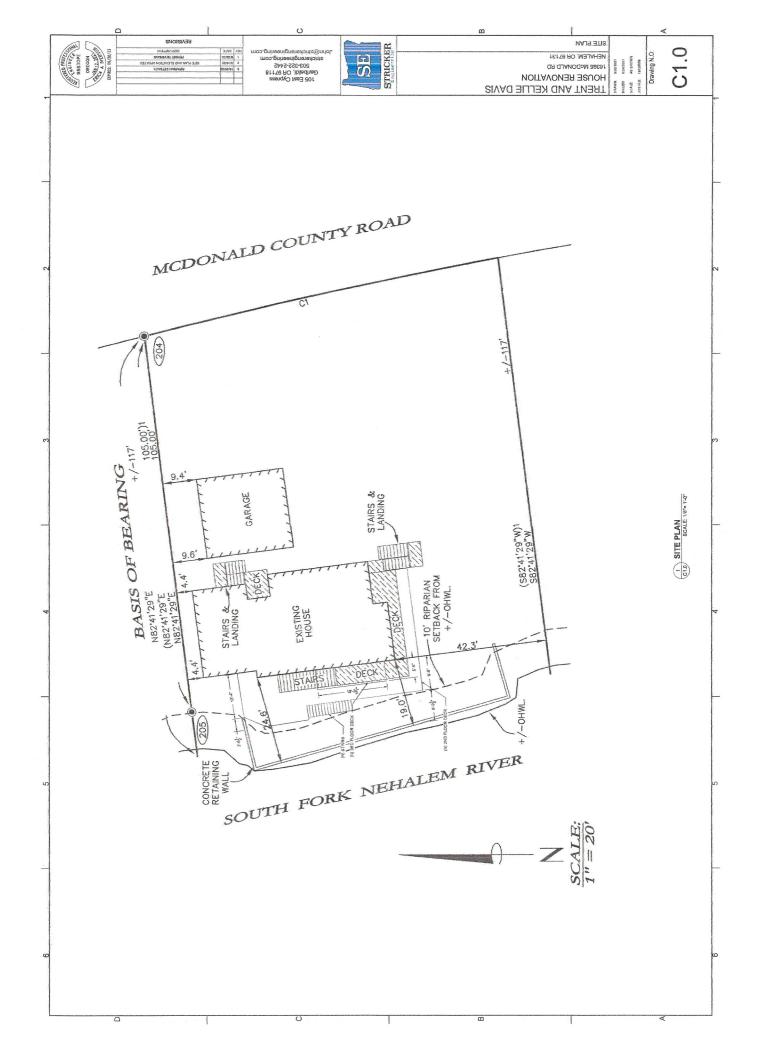
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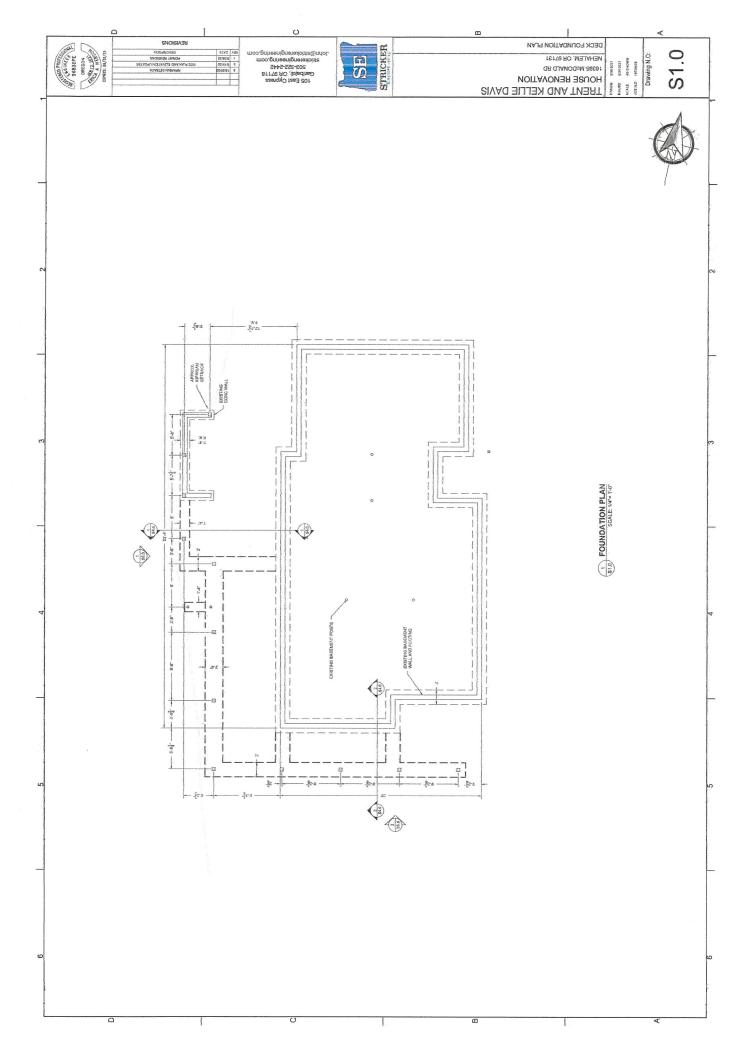
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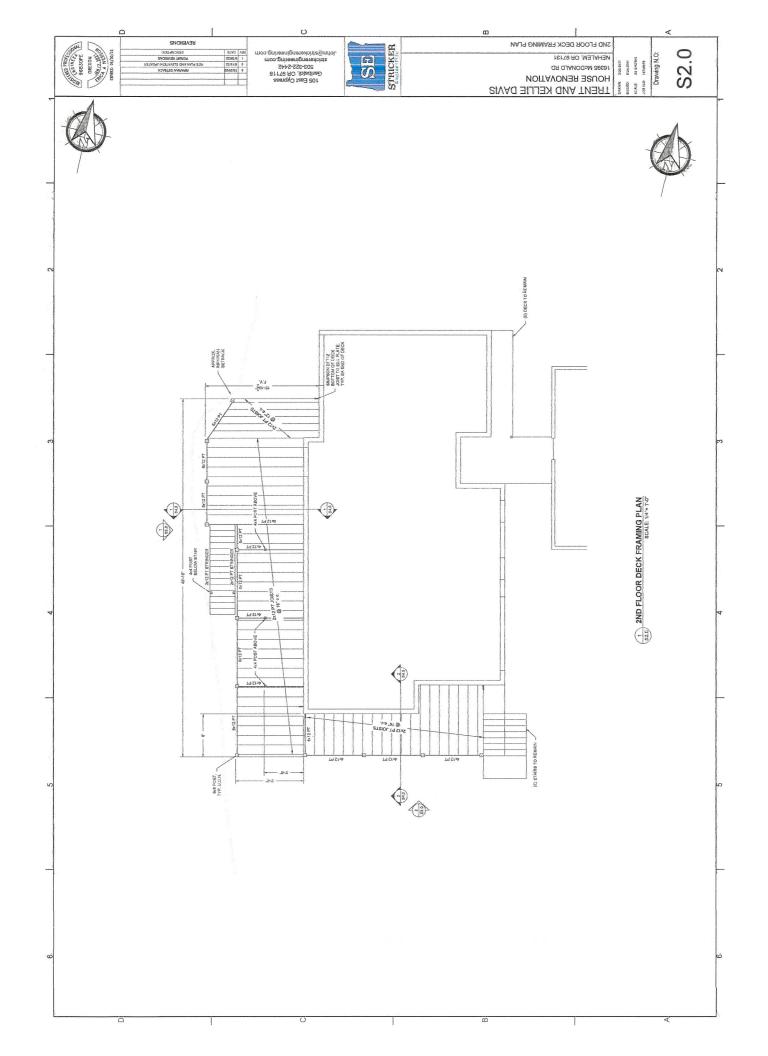
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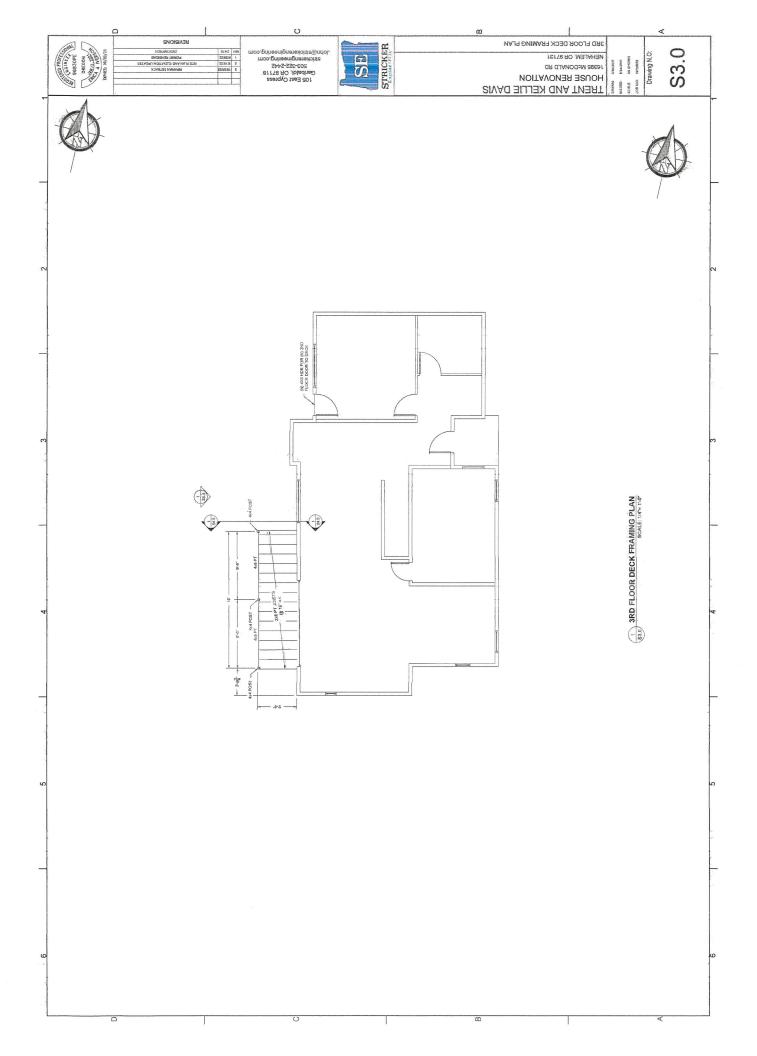
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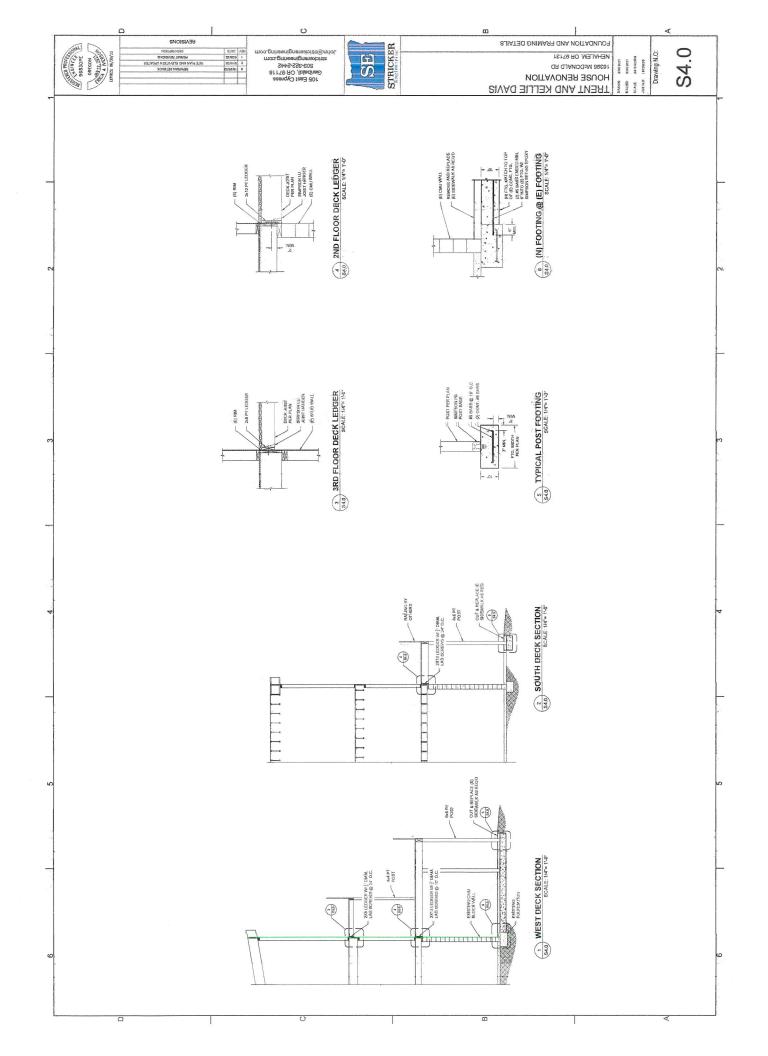
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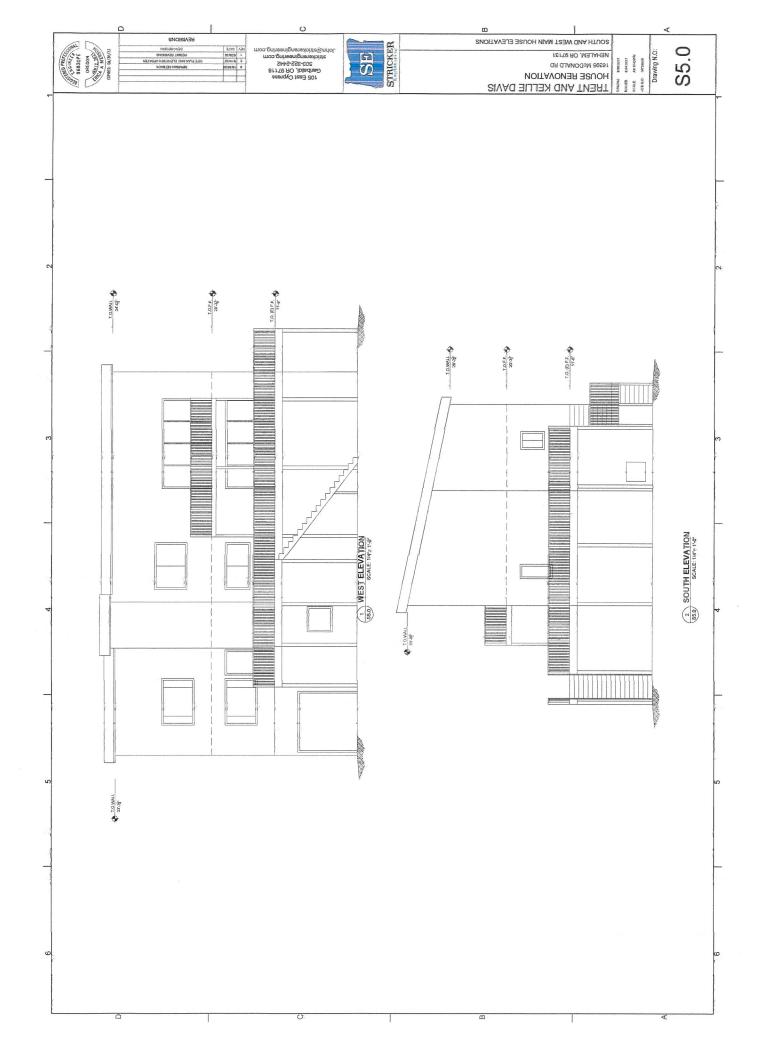












105 East Cypress
Garibaldi, OR 97118
503-322-2442
erica@strickerengineering.com

# Client: Trent & Kellie Davis

Job Description: Deck Addition

Job No: 19726855

**Issued:** 2/1/2022

96830PE
Digitally signed by Erica Iverson
OREGON

EXPIRES: 06/30/23

Stricker Engineering, LLC 105 East Cypress Garibaldi, OR 97118 503-322-2442 erica@strickerengineering.com

# Table of Contents

Structural Design Notes	Project Description	3
Gravity Design		
Deck Framing Design		
Foundation Design	• -	

# Stricker Engineering, LLC

105 East Cypress Garibaldi, OR 97118 503-322-2442 erica@strickerengineering.com

# **Project Description**

This project includes the structural design of an addition to the existing deck at 16395 McDonald Rd in Nehalem, OR. Wood joists and beams are used for the deck framing.

# Structural Design Notes

Loading Criteria:

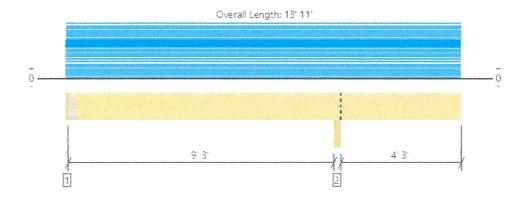
DL = 12.0 psf

LL = 60.0 psf





# Level, Floor: DJ1 1 piece(s) 2 x 12 HF No.2 @ 16" OC



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	435 @ 1 1/2"	911 (1.50")	Passed (48%)		1.0 D + 1.0 L (Alt Spans)
Shear (lbs)	446 @ 8' 5 1/4"	1688	Passed (26%)	1.00	1.0 D + 1.0 L (All Spans)
Moment (Ft-lbs)	983 @ 4' 7 13/16"	2577	Passed (38%)	1.00	1.0 D + 1.0 L (Alt Spans)
Live Load Defl. (in)	0.107 @ 13' 11"	0.220	Passed (2L/982)		1:0 D + 1:0 L (Alt Spans)
Total Load Defl. (in)	0.111 @ 13' 11"	0.440	Passed (2L/954)		1.0 D + 1.0 L (Alt Spans)
TJ-Pro™ Rating	N/A	N/A	N/A		N/A

System: Floor Member Type: Joist Building Use: Residential Building Code: IBC 2018 Design Methodology: ASD

- . Deflection criteria: LL (L/480) and TL (L/240).
- Overhang deflection criteria: LL (2L/480) and TL (2L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- ullet A 15% increase in the moment capacity has been added to account for repetitive member usage.
- · Applicable calculations are based on NDS.
- No composite action between deck and joist was considered in analysis.

	Bearing Length			Loads	to Supports		
Supports	Total	Available	Required	Dead	Floor Live	Total	Accessories
1 - Hanger on 11 1/4" HF ledgerOnMasonry	1.50"	Hanger <sup>1</sup>	1.50"	61	386/-72	447/-72	See note 1
2 - Beam - HF	3.50"	3.50"	1.60"	162	810	972	Blocking

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.
- · At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- <sup>1</sup> See Connector grid below for additional information and/or requirements.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	13' 3" o/c	
Bottom Edge (Lu)	13' 10" o/c	

Maximum allowable bracing intervals based on applied load.

Connector: Simpson Strong-1	Tie					
Support	Model	Seat Length	Top Fasteners	Face Fasteners	Member Fasteners	Accessories
1 - Face Mount Hanger	LUS28	1.75"	N/A	6-10dx1.5	3-10d	

Refer to manufacturer notes and instructions for proper installation and use of all connectors.

Vertical Load	Location (Side)	Spacing	Dead (0.90)	Floor Live (1.00)	Comments
1 - Uniform (PSF)	0 to 13' 11"	16"	12.0	60.0	Default Load

## Weyerhaeuser Notes

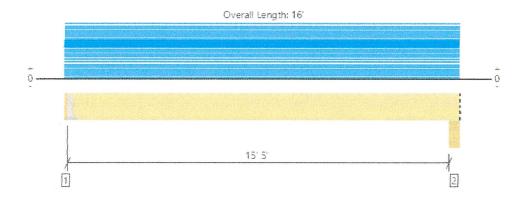
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ForteWEB Software Operator	Job Notes
Erica Iverwon Stricker Engineering (208) 404-4404 erica@strickerengineering.com	





# Level, Floor: DJ2 1 piece(s) 2 x 12 HF No.2 @ 12" OC



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	558 @ 1 1/2"	911 (1.50")	Passed (61%)	T	1.0 D + 1.0 L (All Spans)
Shear (lbs)	491 @ 1' 3/4"	1688	Passed (29%)	1.00	1.0 D + 1.0 L (All Spans)
Moment (Ft-lbs)	2162 @ 7' 10 1/2"	2577	Passed (84%)	1.00	1.0 D + 1.0 L (All Spans)
Live Load Defl. (in)	0.337 @ 7' 10 1/2"	0.387	Passed (L/552)		1:0 D + 1:0 L (All Spans)
Total Load Defl. (in)	0.404 @ 7' 10 1/2"	0.775	Passed (L/460)		1.0 D + 1.0 L (All Spans)
TJ-Pro™ Rating	N/A	N/A	N/A		N/A

System: Floor Member:Type: Joist. Building Use: Residential Building Code: IBC 2018 Design Methodology: ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A 15% increase in the moment capacity has been added to account for repetitive member usage.
- · Applicable calculations are based on NDS.
- · No composite action between deck and joist was considered in analysis.

	Bearing Length			Loads	to Supports (		
Supports	Total	Available	Required	Dead	Floor Live	Total	Accessories
1 - Hanger on 11 1/4" HF ledgerOnMasonry	1.50"	Hanger <sup>1</sup>	1.50"	95	473	568	See note <sup>1</sup>
2 - Beam - HF	5.50"	5.50"	1.50"	98	488	586	Blocking

- · Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.
- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ¹ See Connector grid below for additional information and/or requirements.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	4' 5" o/c	
Bottom Edge (Lu)	15' 11" o/c	

<sup>•</sup>Maximum allowable bracing intervals based on applied load.

Connector: Simpson Strong-1	îe .					
Support	Model	Seat Length	Top Fasteners	Face Fasteners	Member Fasteners	Accessories
1 - Face Mount Hanger	LUS28	1.75"	N/A	6-10dx1.5	3-10d	

<sup>·</sup> Refer to manufacturer notes and instructions for proper installation and use of all connectors.

Vertical Load	Location (Side)	Spacing	Dead (0.90)	Floor Live (1.00)	Comments
1 - Uniform (PSF)	0 to 16'	12"	12.0	60.0	Default Load

### Weyerhaeuser Notes

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

ForteWEB Software Operator	Job Notes	
Erica Iverwon Stricker Engineering (208) 404-4404 erica@strickerengineering.com	*	



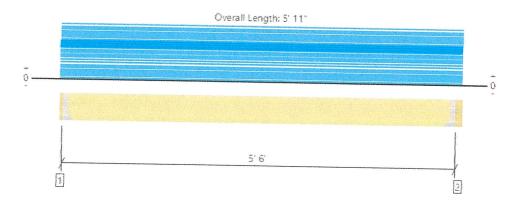
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ForteWEB v3.2, Engine: V8.2.0.17, Data: V8.1.0.16



### MEMBER REPORT

# Level, Floor: DJ3 1 piece(s) 2 x 8 HF No.2 @ 16" OC



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	264 @ 1 1/2"	911 (1.50*)	Passed (29%).		1.0 D + 1.0 L (All Spans)
Shear (lbs)	206 @ 8 3/4"	1088	Passed (19%)	1.00	1.0 D + 1.0 L (All Spans)
Moment (Ft-lbs)	363 @ 2' 10 1/2"	1284	Passed (28%)	1.00	1.0 D + 1.0 L (All Spans)
Live Load Defl. (in)	0.027 @ 2' 10 1/2"	0.138	Passed (L/9994)		1:0 D + 1:0 L (All Spans)
Total Load Defl. (in)	0.032 @ 2' 10 1/2"	0.275	Passed (L/999+)		1.0 D + 1.0 L (All Spans)
TJ-Pro™ Rating	N/A	N/A	N/A	<b></b> -	N/A

System: Floor Member: Type: Joist Building Use: Residential Building Code: IBC 2018 Design Methodology: ASD

- Deffection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A 15% increase in the moment capacity has been added to account for repetitive member usage.
- · Applicable calculations are based on NDS.
- No composite action between deck and joist was considered in analysis.

	Bearing Length			Loads	to Supports (		
Supports	Total Available Required		Dead Floor Live Total		Total	Accessories	
1 - Hanger on 7 1/4" HF ledgerOnMasonry	1.50"	Hanger <sup>1</sup>	1.50"	46	230	276	See note 1
2 - Hanger on 7 1/4" HF beam	3.50"	Hanger <sup>1</sup>	1.50"	49	243	292	See note 1

- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ¹ See Connector grid below for additional information and/or requirements.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	5' 6" o/c	
Bottom Edge (Lu)	5' 6" o/c	

Maximum allowable bracing intervals based on applied load.

Connector: Simpson Strong	-Tie					
Support	Model	Seat Length	Top Fasteners	Face Fasteners	Member Fasteners	Accessories
1 - Face Mount Hanger	LU26	1.50"	N/A	6-10dx1.5	4-10dx1.5	Accessories
2 - Face Mount Hanger	LU26	1.50"	N/A	6-10dx1.5	4-10dx1.5	-

Refer to manufacturer notes and instructions for proper installation and use of all connectors.

Vertical Load	Location (Side)	Spacing	(0.90)	Floor Live (1.00)	Comments
1 - Uniform (PSF)	0 to 5' 11"	16"	12.0	60.0	Default Load

# Weyerhaeuser Notes

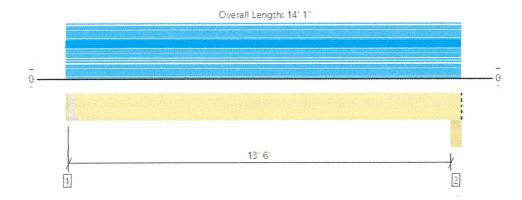
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ForteWEB Software Operator	Job Notes	
Erica Iverwon Stricker Engineering (208) 404-4404 erica@strickerengineering.com		





# Level, Floor: DJ4 1 piece(s) 2 x 12 HF No.2 @ 16" OC



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	652 @ 1 1/2*	911 (1.50")	Passed (72%)		1.0 D + 1.0 L (All Spans)
Shear (lbs)	562 @ 1' 3/4"	1688	Passed (33%)	1.00	1.0 D + 1.0 L (All Spans)
Moment (Ft-lbs)	2214 @ 6' 11"	2577	Passed (86%)	1.00	1.0 D + 1.0 L (All Spans)
Live Load Defl. (in)	0.265 @ 6" 11"	0.340	Passed (L/615)	==	1:0 D + 1:0 L (All Spans)
Total Load Defl. (in)	0.318 @ 6' 11"	0.679	Passed (L/513)	T	1.0 D + 1.0 L (All Spans)
TJ-Pro™ Rating	N/A	N/A	N/A		N/A

System: Floor Member: Type: Joist Building Use: Residential Building Code: IBC 2018 Design Methodology: ASD

- Deflection criteria: LL (L/480) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- A 15% increase in the moment capacity has been added to account for repetitive member usage.
- Applicable calculations are based on NDS.
- No composite action between deck and joist was considered in analysis.

		Bearing Length			to Supports		
Supports	Total	Available	Required	Dead	Floor Live	Total	Accessories
1 - Hanger on 11 1/4" HF beam	1.50"	Hanger <sup>1</sup>	1.50"	111	553	664	See note 1
2 - Beam - HF	5.50"	5.50°	1.50"	115	573	688	Blocking

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.
- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- 1 See Connector grid below for additional information and/or requirements.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	4' 2" o/c	
Bottom Edge (Lu)	14' o/c	

<sup>•</sup>Maximum allowable bracing intervals based on applied load.

Connector: Simpson Strong-Tie								
Support	Model	Seat Length	Top Fasteners	Face Fasteners	Member Fasteners	Accessories		
1 - Face Mount Hanger	LUS28	1.75"	N/A	6-10dx1.5	3-10d			

Refer to manufacturer notes and instructions for proper installation and use of all connectors.

Vertical Load	Location (Side)	Spacing	Dead (0.90)	Floor Live (1.00)	Comments
1 - Uniform (PSF)	0 to 14' 1"	16"	12.0	60.0	Default Load

### Weyerhaeuser Notes

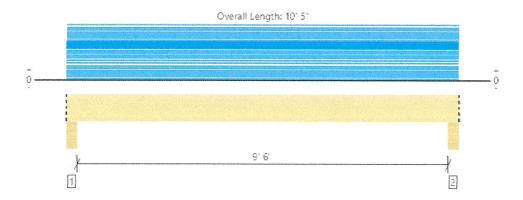
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ForteWEB Software Operator	Job Notes	
Erica Iverwon Stricker Engineering (208) 404-4404 erica@strickerengineering.com		





# Level, Floor: DB1 1 piece(s) 6 x 12 HF No.2



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	2490 @ 4**	12251 (5.50")	Passed (20%)		1.0 D+ 1.0 L (All Spans)
Shear (lbs)	1812 @ 1' 5"	5903	Passed (31%)	1.00	1.0 D + 1.0 L (All Spans)
Moment (Ft-lbs)	5680 @ 5' 2 1/2"	6819	Passed (83%)	1.00	1.0 D + 1.0 L (All Spans)
Live Load Defl. (in)	0.102 @ 5' 2 1/2"	0.325	Passed (L/999+)		1:0 D + 1:0 L (All Spans)
Total Load Defl. (in)	0.127 @ 5' 2 1/2"	0.488	Passed (L/923)		1.0 D + 1.0 L (All Spans)

System : Floor Member Type : Drop Beam. Building Use : Residential

Building Ose: Residential Building Code: IBC 2018 Design Methodology: ASD

- Deflection criteria: LL (L/360) and TL (L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Lumber grading provisions must be extended over the length of the member per NDS 4.2.5.5.
- Applicable calculations are based on NDS.

		Bearing Length			to Supports (		
Supports	Total	Available	Required	Dead	Floor Live	Total	Accessories
1 - Column - HF	5.50"	5.50"	1.50"	484	2005	2489	Blocking
2 - Column - HF	5.50"	5.50"	1.50"	484	2005	2489	Blocking

Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	10' 5" o/c	
Bottom Edge (Lu)	10° 5" o/c	

Maximum allowable bracing intervals based on applied load.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Floor Live (1.00)	Comments
0 - Self Weight (PLF)	0 to 10' 5"	N/A	16.0	-	
1 - Uniform (PSF)	0 to 10' 5" (Front)	6' 5"	12.0	60.0	

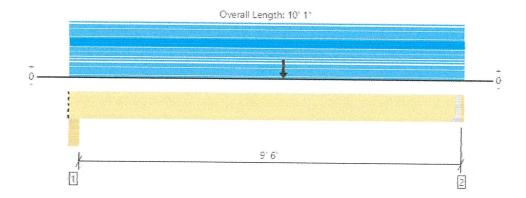
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ForteWEB Software Operator	Job Notes	
Erica Iverwon Stricker Engineering (208) 404-4404 erica@strickerengineering.com		



# Level, Floor: DB2 1 piece(s) 4 x 12 HF No.2



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	1366 @ 9' 11 1/2"	2126 (1.50")	Passed (64%)	T	1.0 D + 1.0 L (All Spans)
Shear (lbs)	1266 @ 9' 1/4"	3938	Passed (32%)	1.00	1.0 D + 1.0 L (All Spans)
Moment (Ft-lbs)	5035 @ 5' 6"	5752	Passed (88%)	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	
Live Load Defl. (in)	0.105 @ 5' 2 1/2"	0.321	Passed (L/999+)	-	1.0 D + 1.0 L (All Spans)
Total Load Defl. (in)	0.132 @ 5' 2 1/2"	0.481	Passed (L/875)	-	1.0 D + 1.0 L (All Spans)

System: Floor

Member Type : Drop Beam Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD

- Deflection criteria: LL (L/360) and TL (L/240).
- · Allowed moment does not reflect the adjustment for the beam stability factor.
- · Applicable calculations are based on NDS.

Piller Commencer (1991) and the company of the	Bearing Length			Loads to Supports (lbs)			
Supports	Total	Available	Required	Dead	Floor Live	Total	Accessories
1 - Column - HF	5.50"	5.50"	1.50"	274	1010	1284	Blocking
2 - Hanger on 11 1/4" HF ledgerOnMasonry	1.50"	- Hanger <sup>1</sup>	1.50™	289	1088	1377	See note 1

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.
- · At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ¹ See Connector grid below for additional information and/or requirements.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	10' o/c	
Bottom Edge (Lu)	10' o/c	

Maximum allowable bracing intervals based on applied load.

Connector: Simpson Strong-Tie								
Support	Model	Seat Length	Top Fasteners	Face Fasteners	Member Fasteners	Accessories		
2 - Face Mount Hanger	HUS410	2.00"	N/A	8-10dx1,5	8-10d			

Refer to manufacturer notes and instructions for proper installation and use of all connectors.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Floor Live (1.00)	Comments
0 - Self Weight (PLF)	0 to 9' 11 1/2"	N/A	10.0		
1 - Uniform (PSF)	0 to 10' 1" (Top)	1' 4"	12.0	60.0	
2 - Point (lb)	5' 6" (Top)	N/A	302	1292	Linked from: Floor: DB5, Support 1

### **Weyerhaeuser Notes**

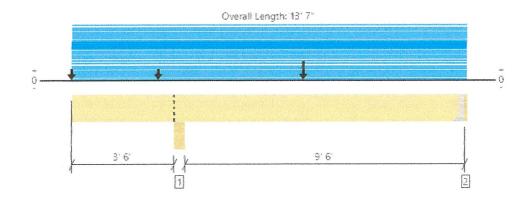
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ForteWEB Software Operator	Job Notes	
Erica Iverwon Stricker Engineering (208) 404-4404 erica@strickerengineering.com		





#### Level, Floor: DB3 1 piece(s) 4 x 12 HF No.2



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	1162 @ 13' 5 1/2"	2126 (1.50")	Passed (55%)		1.0 D + 1.0 L (Alt Spans)
Shear (lbs)	1568 @ 4' 10 3/4"	3938	Passed (40%)	1.00	1.0 D + 1.0 L (All Spans)
Moment (Ft-lbs)	4765 @ 8'	5752	Passed (83%)	1.00	1.0 D + 1.0 L (Alt Spans)
Live Load Defl. (in)	0.114 @ 0	0.249	Passed (2L/784)		1:0 D + 1:0 L (Alt Spans)
Total Load Defl. (in)	0.107 @ 0	0.373	Passed (2L/838)		1.0 D + 1.0 L (Alt Spans)

System: Floor Member Type: Drop Beam Building Use: Residential Building Code: IBC 2018 Design Methodology: ASD

- Deflection criteria: LL (L/360) and TL (L/240).
- Overhang deflection criteria: LL (2L/360) and TL (2L/240).
- Allowed moment does not reflect the adjustment for the beam stability factor.
- Applicable calculations are based on NDS.

	Bearing Length			Loads	to Supports (	Conf. Contract Contract		
Supports	Total Avail	Available	Required	Dead	Floor Live	Total	Accessories	
1 - Column - HF	5.50"	5.50"	2.11"	596	2391	2987	Blocking	
2 - Hanger on 11 1/4" HF ledgerOnMasonry	1.50"	Hanger <sup>1</sup>	1.50"	208	966/-219	1174/- 219	See note 1	

- Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.
- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- 1 See Connector grid below for additional information and/or requirements.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	13' 6" o/c	
Bottom Edge (Lu)	13' 6" o/c	

<sup>•</sup>Maximum allowable bracing intervals based on applied load.

Connector: Simpson Strong-Tie									
Support	Model	Seat Length	Top Fasteners	Face Fasteners	Member Fasteners	Accessories			
2 - Face Mount Hanger	LUS414	2.00"	N/A	10-10dx1.5	6-10d				

Refer to manufacturer notes and instructions for proper installation and use of all connectors.

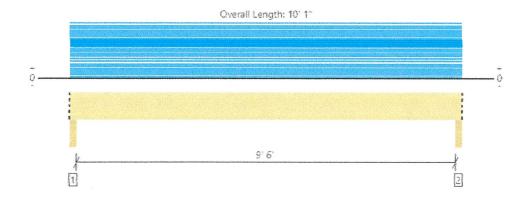
Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Floor Live (1.00)	Comments
0 - Self Weight (PLF)	0 to 13"5 1/2"	N/A	10.0		l.
1 - Uniform (PSF)	0 to 13' 7" (Top)	1' 4"	12.0	60.0	
2 - Point (lb)	0 (Front)	N/A	75	375	<b>X</b>
3 - Point (lb)	3' (Front)	N/A	75	375	
4 - Point (lb)	8' (Top)	N/A	302	1292	Linked from: Floor: DB5, Support 1

ForteWEB Software Operator.	Job Notes	
Erica Iverwon Stricker Engineering (208) 404-4404 erica@strickerengineering.com		





#### Level, Floor: DB4 1 piece(s) 6 x 12 HF No.2



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	2561 @ 2"	7796 (3.50")	Passed (33%)	I -	1.0 D + 1.0 L (All Spans)
Shear (lbs)	1926 @ 1' 3"	5903	Passed (33%)	1.00	1.0 D + 1.0 L (All Spans)
Moment (Ft-lbs)	6036 @ 5' 1/2"	6819	Passed (89%)	1.00	1.0 D + 1.0 L (All Spans)
Live Load Defl. (in)	0.109 @ 5' 1/2"	0.325	Passed (L/999+)	-	1.0 D + 1.0 L (All Spans)
Total Load Defl. (in)	0.135 @ 5' 1/2"	0.488	Passed (L/869)	-	1.0 D + 1.0 L (All Spans)

System: Floor
Member Type: Drop Beam
Building Use: Residential
Building Code: IBC 2018
Design Methodology: ASD

- Deflection criteria: LL (L/360) and TL (L/240).
- · Lumber grading provisions must be extended over the length of the member per NDS 4.2.5.5.
- · Applicable calculations are based on NDS.

		Bearing Length			to Supports	action of the other office	
Supports	Total	Available	Required	Dead	Floor Live	Total	Accessories
1 - Column - DF	3.50"	3.50"	1.50"	494	2067	2561	Blocking
2 - Column - DF	3.50"	3.50"	1.50"	494	2067	2561	Blocking

. Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	Continuous	
Bottom Edge (Lu)	All Bearing Points	

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Floor Live (1.00)	Comments
0 - Self Weight (PLF)	0 to 10' 1"	N/A	16.0	-	
1 - Uniform (PSF)	0 to 10' 1" (Front)	6' 10"	12.0	60.0	

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator





#### Level, Floor: DB5 1 piece(s) 4 x 12 HF No.2



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	1594 @ 2"	4961 (3.50")	Passed (32%)	-	1.0 D + 1.0 L (All Spans)
Shear (lbs)	1151 @ 1' 2 3/4"	3938	Passed (29%)	1.00	1.0 D + 1.0 L (All Spans)
Moment (Ft-lbs)	3260 @ 4' 5"	5752	Passed (57%)	1.00	1.0 D + 1.0 L (All Spans)
Live Load Defl. (in)	0.064 @ 4' 5"	0.283	Passed (L/999+)	-	1.0 D + 1.0 L (All Spans)
Total Load Defl. (in)	0.079 @ 4' 5"	0.425	Passed (L/999+)		1.0 D + 1.0 L (All Spans)

System: Floor Member Type : Drop Beam Building Use: Residential Building Code: IBC 2018 Design Methodology: ASD

- Deflection criteria: LL (L/360) and TL (L/240).
- · Applicable calculations are based on NDS.

		Bearing Length			to Supports (		
Supports	Total	Available	Required	Dead	Floor Live	Total	Accessories
1 - Column - DF	3.50"	3.50"	1.50"	302	1292	1594	Blocking
2 - Column - DF	3.50"	3.50"	1.50"	302	1292	1594	Blocking

Blocking Panels are assumed to carry no loads applied directly above them and the full load is applied to the member being designed.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	Continuous	
Bottom Edge (Lu)	All Bearing Points	

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Floor Live (1.00)	Comments
0 - Self Weight (PLF)	0 to 8' 10"	N/A	10:0		
1 - Uniform (PSF)	0 to 8' 10" (Front)	4' 10 1/2"	12.0	60.0	1

#### Weyerhaeuser Notes

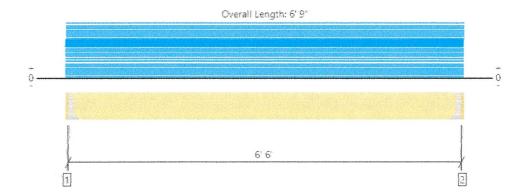
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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator





#### Level, Floor: DB6 1 piece(s) 4 x 8 HF No.2



All locations are measured from the outside face of left support (or left cantilever end). All dimensions are horizontal.

Design Results	Actual @ Location	Allowed	Result	LDF	Load: Combination (Pattern)
Member Reaction (lbs)	781 @ 1 1/2"	2126 (1.50")	Passed (37%)	l -	1.0 D + 1.0 L (All Spans)
Shear (lbs)	636 @ 8 3/4"	2538	Passed (25%)	1.00	1.0 D + 1.0 L (All Spans)
Moment (Ft-lbs)	1270 @ 3' 4 1/2"	2823	Passed (45%)	1.00	1.0 D + 1.0 L (All Spans)
Live Load Defl. (in)	0.054 @ 3' 4 1/2"	0.217	Passed (L/999+)	-	1.0 D + 1.0 L (All Spans)
Total Load Defl. (in)	0.067 @ 3' 4 1/2"	0.325	Passed (L/999+)		1.0 D + 1.0 L (All Spans)

Member Type : Drop Beam Building Use : Residential Building Code : IBC 2018 Design Methodology : ASD

System: Floor

- Deflection criteria: LL (L/360) and TL (L/240).
- · Applicable calculations are based on NDS.

TANKER OF USER SECTION	Bearing Length			Loads to Supports (lbs)			Carrier Green Committee Committee
Supports	Total	Available	Required	Dead	Floor Live	Total	Accessories
1 - Hanger on 7 1/4" HF ledgerOnMasonry	1.50"	Hanger <sup>1</sup>	1.50"	153	658	811	See note 1
2 - Hanger on 7 1/4" HF ledgerOnMasonry	1.50"	Hanger <sup>1</sup>	1.50"	153	658	811	See note 1

- At hanger supports, the Total Bearing dimension is equal to the width of the material that is supporting the hanger
- ¹ See Connector grid below for additional information and/or requirements.

Lateral Bracing	Bracing Intervals	Comments
Top Edge (Lu)	Continuous	
Bottom Edge (Lu)	All Bearing Points	

Connector: Simpson Strong-Tie						
Support	Model	Seat Length	Top Fasteners	Face Fasteners	Member Fasteners	Accessories
1 - Face Mount Hanger	LUS48	2.00"	N/A	6-10dx1.5	4-10d	
2 - Face Mount Hanger	LUS48	2.00"	N/A	6-10dx1.5	4-10d	

<sup>·</sup> Refer to manufacturer notes and instructions for proper installation and use of all connectors.

Vertical Loads	Location (Side)	Tributary Width	Dead (0.90)	Floor Live (1.00)	Comments
0 - Self Weight (PLF)	1 1/2" to 6' 7 1/2"	N/A	6.4	-	
1 - Uniform (PSF)	0 to 6' 9" (Front)	3° 3″	12.0	60.0	

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The product application, input design loads, dimensions and support information have been provided by ForteWEB Software Operator

ForteWEB Software Operator	Job Notes	75
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#### Stricker Engineering, LLC

105 East Cypress Garibaldi, OR 97118 503-322-2442 erica@strickerengineering.com

#### Foundation Design

#### WF1:

$$\begin{split} W_{DL} &= 15 \text{ psf*}(28'/2)*3 + 12 \text{ psf*}(9.5'/2+5'/2) + 57 \text{ psf*}11.5' = 1379 \text{ plf} \\ W_{SL} &= 25 \text{ psf*}(28'/2+1') = 375 \text{ plf} \\ W_{RLL} &= 20 \text{ psf*}(28'/2+1') = 300 \text{ plf} \\ W_{LL} &= 40 \text{ psf*}(28'/2)*2 + 60 \text{ psf*}(9.5'/2+6'/2) = 1585 \text{ plf} \\ W_{TL} &= 1379 \text{ plf} + 300 \text{ plf} + 1585 \text{ plf} = 3282 \text{ plf} \\ W_{req'd} &= 3282 \text{ plf/} 1500 \text{ psf} = 2.18 \text{ ft} \end{split}$$

#### Use minimum 2'-0" wide wall footing

#### F1:

$$W_{DL}$$
 = 484 lbs\*2 (DB1 Reaction) + 538 lbs (DB3 Reaction) = 1506 plf   
 $W_{LL}$  = 2005 lbs\*2 (DB1 Reaction) + 2133 lbs = 6143 plf   
 $W_{TL}$  = 1506 plf + 6143 plf = 7649 plf   
 $W_{reg'd}$  = 7649 plf/ 1500 psf = 5.10 ft

#### Use minimum 2'-6" square footing

#### **₹2**:

$$W_{DL}$$
 = 484 lbs (DB1 Reaction) + 575 lbs (DB4 Reaction) = 1059 plf  $W_{TL}$  = 2005 lbs (DB1 Reaction) + 2402 lbs = 4407 plf  $W_{TL}$  = 1059 plf + 4407 plf = 5466 plf  $W_{req'd}$  = 5466 plf/ 1500 psf = 3.64 ft

#### Use minimum 2'-0" square footing

#### Stricker Engineering, LLC

105 East Cypress Garibaldi, OR 97118 503-322-2442

#### erica@strickerengineering.com

#### Lateral Design

Deck Calculator: Lateral	Loads				
Vind Analysis Method		Design Wind Loa	ds - Other Structures	ASCE 7-10 Sec. 29.5	
Basic Wind Speed (ultimate		500 gr 110 250	135.00 MPH		
Topography Factor	,	Kzt =	1.00	ASCE 7-16 Fig. 26.8-	1
Directionality Factor		Kd =	0.85	ASCE 7-16 Fig. 26.6-	
Gust Effect Factor		G=	0.85	ASCE 7-16 Sec. 26.9	
Deck Height		h=	11.50 ft	710021 2000.200	
and the second s			C	a =	9.5
errain Exp. Category	ffiniont	Kz=	0.849	zg =	900
elocity Pressure Exp. Coe	HICIEIL	1/2 -	0.043	29	000
elocity Pressure		qz =	33.66 psf	qz = .00256Kz R	Kzt Kd V <sup>2</sup>
eck Gross Area (normal to	wind)	Agross =	50.00 ft <sup>2</sup>		
eck Solid Area (normal to w	ind)	Af =	200.00 ft <sup>2</sup>		
atio of Solid Area to Gros	s Area	€=	4.00		
orce Coefficient for Deck		Of,deck =	1.85	ASCE 7-16 Fig. 29.4-	2
Vind Load on Deck		Fdeck =	10,588 lbs	$F = q_z GC_t A_t$	
SD Wind Load on Deck		FASD,deck =	6,353 lbs		
lost Height		hposi =	10.50 ft	Post Section: SC	UARE
ost Width or Dia.		D=	5.50 in		
eck Post Area		Af =	4.81 ft <sup>2</sup>		
ost Aspect Ratio		h/D =	22.91		
orce Coefficient for Post		Cf.post =	1.85	ASCE 7-10 Fig. 29.5-	-1
Vind Load on Post		Fpost =	255 lbs	$F = q_{x}GC_{t}A_{t}$	
SD Wind Load on Post		FASD,post =	153 lbs		
otal ASD Wind Load		FASD,WIND =	6,429 lbs		
Deck Width (perpendicular	to ledger)	B=	15.83 ft	Deck Ratio:	0.32
Deck Length (parallel to ledg	jer)	L=	50.00 ft	Deck Area:	791.65 ft <sup>2</sup>
Deck Moments	(wind)		51,500 ft-lbs		
eck Holdown Force	(wind)	Fh,WIND =	1,030 lbs		
hit Shear @ Ledger	(wind)	V <sub>M</sub> =	129 plf		
eck Live Load		LL=	60.00 psf	ρ =	1.3 (SDC D)
eck Dead Load		DL =	12.00 psf	· vocate	
Other Loads			0 lbs	(Conservatively incl	ude live loads in Effectiv
Effective Seismic Weight		W=	56,999 lbs	Seismic Weight)	
Seismic Response Coeffic	ient	Cs =	0,151	(from Seismic Work	sheet)
ciamic reaponae coemo	ione	0.0		$E_b = 0.7 pC_s W$	
Total ASD Seismic Load	F	ASD,SEISM IC =	7,832 lbs	(governs)	
Deck Moments	(seismic)		62,004 ft-lbs		
Deck Holdown Force	(seismic)	Fh,SEISMIC =	1,240 lbs	(governs)	
Init Shear @ Ledger	(seismic)	v <sub>s</sub> =	157 plf	(governs)	
Deck Area		Adeck =	792 ft <sup>2</sup>		
Occupant Lateral Load per	Plan Area	OL=	5.00 psf		ateral Loading by Occupa
Total ASD Occupant Load		FASD,OCC=	3,958 lbs	Donald A. Bender, 2	O NI
			21 22E # lba		
Deck Moments	(occupants)	D	31,335 ft-lbs		
Deck Holdown Force	(occupants)	Fh,occ =	627 lbs		
Unit Shear @ Ledger	(occupants)	V =	79. plf		



#### **NO-RISE CERTIFICATION AND REPORT**

Nehalem River at McDonald Dike Road Nehalem, Oregon

Prepared for:

Trent and Kellie Davis 16395 McDonald Dike Road Nehalem, Oregon 97131

Prepared by:

Cascade Water Resources, LLC

March 6, 2023

Project No. 1026



Project No.: 1026

March 6, 2023 Project No. 1026

Trent and Kellie Davis 16395 McDonald Dike Road Nehalem, Oregon 97131

Via email: Trent-davis@outlook.com

Attention: Trent and Kellie Davis

Subject: No-Rise Report and Certification for Nehalem River at McDonald Dike Road

Nehalem, Oregon 97131

#### Dear Trent and Kellie:

The following report documents Cascade Water Resources, LLC's (CWR's) finding that the proposed construction of a new deck at the property located at 16395 McDonald Dike Road as described on the Stricker Engineering construction plans dated October 25, 2022 will not increase the 100-year (1%-annual chance) pre-project base flood elevations, floodway elevations, or floodway widths on Nehalem River at published or unpublished cross-sections as shown on the Flood Insurance Study for Tillamook County, Oregon dated September 28, 2018 (FEMA, 2018).

The report includes tables and figures that document our analysis. Model input (cross-sections) and output data are appended to the report along with copies of the drawings provided by Stricker Engineering. Digital copies of the hydraulic model and work map are also provided for your reference.

We appreciate this opportunity to be of service. Please feel free to contact me if you have any questions regarding this report.

Sincerely,

Roger Sutherland, PE

Cascade Water Resources, LLC

P.C.



# No-Rise Engineering Certification Nehalem River at 16395 McDonald Dike Road Nehalem, Oregon March 6, 2023

This is to certify that I am a duly qualified registered professional engineer licensed to practice in the State of Oregon. This is further to certify that the attached report supports the finding that the proposed construction of a new deck at the property located at 16395 McDonald Dike Road in Nehalem, Oregon, as described on the Stricker Engineering construction plans dated October 25, 2022, will not increase the 100-year (1%-annual chance) pre-project base flood elevations, floodway elevations, or floodway widths on Nehalem River at published or unpublished cross-sections as shown on the Flood Insurance Study for Tillamook County, Oregon dated September 28, 2018 (FEMA, 2018). In addition to this report and its attachments, a hydraulic model and work map are provided to support the finding that this proposed project will meet no-rise criteria.

This certification was prepared exclusively for Trent and Kellie Davis. The quality of information, conclusions, and estimates contained herein is consistent with the level of effort involved in CWR services and based on:1) a field visit to the site on May 17, 2022; 2) information available at the time of preparation; 3) data supplied by outside sources; and 4) the assumptions, conditions, and qualifications set forth in this report. This No-Rise Certification is intended to be used by Trent and Kellie Davis for the McDonald Dike Road deck project only, subject to the terms and conditions of its contract with CWR. Any other use of, or reliance on, this report by any third party is at that party's sole risk.

While this report was prepared in accordance with standard engineering practice by qualified engineering professionals, this report evaluated a specific storm recurrence interval and assumes free-flowing hydraulic conditions. It is reasonable to assume that a storm event of greater magnitude or changes in water-way conveyance capacity might cause higher stages than estimated for this assignment.

March 6, 2023

Project No.: 1026

Roger Sutherland, PE

Cascade Water Resources, LLC

Expires: 6/30/2024



#### **TABLE OF CONTENTS**

			Page
1.0	SUM	IMARY	1
2.0		JECT DESCRIPTIONFEMA Effective Flood Model Proposed Floodway Development	1
3.0	NO-R 3.1 3.2 3.3 3.4 3.5	RISE HYDRAULIC MODELING  Duplicate Effective Model  Corrected Effective Modef  Existing (Pre-Project) Conditions Model  Proposed Conditions Model  No-Rise Results	2 4 5
4.0 REFE		CLUSIONS	6
LIMITA	NOITA	S	8

#### **TABLE**

Table 1: No-Rise Analysis

#### **FIGURES**

Figure 1: Study Area Vicinity

Figure 2: Flood Insurance Rate Map Panel

Figure 3: Hydraulic Model Work Map

Figure 4: FEMA FIRMette

#### **APPENDICES**

Appendix A	Corrected Effective / Pre-Project Conditions Hydraulic Model Output
Appendix B	Proposed Conditions Hydraulic Model Output
Appendix C	Proposed Deck Construction Plans by Stricker Engineering
Appendix D	Photo Log



### NO-RISE REPORT Nehalem River at 16395 McDonald Dike Road Nehalem, Oregon

#### 1.0 SUMMARY

Project No.: 1026

Cascade Water Resources, LLC (CWR) found that the proposed construction of a new deck at the property located at 16395 McDonald Dike Road in Nehalem, Oregon meets the no-rise requirement if constructed as described on the Stricker Engineering construction plans dated October 25, 2022. The construction plans are included in Appendix C.

#### 2.0 PROJECT DESCRIPTION

#### 2.1 FEMA EFFECTIVE FLOOD MODEL

WEST Consultants, Inc. (WEST) completed a Letter of Map Revision (LOMR) for the Lower Nehalem River in Tillamook County, Oregon, in 2014. The LOMR update extended from the Federal Emergency Management Agency (FEMA) Cross-Section B at model river station 0.45 to Cross-Section O at model river station 6.80. The river stations represent miles along the Nehalem River centerline. WEST used 2009 lidar data from the Oregon Department of Geology and Mineral Industries (DOGAMI) to update existing cross-section overbank data and to create additional cross-sections that were used in the detailed analysis. The LOMR was used to update a 2002 FEMA Flood Insurance Study (FIS) and represents the best available information and serves as the FEMA effective model for the Lower Nehalem River (WEST, 2014). The LOMR produced by WEST was ultimately incorporated into a September 28, 2018, FIS update for Tillamook County, Oregon. Figure 2 shows the Flood Insurance Rate Map (FIRM) Panel 41057C0230F issued for Tillamook County as part of the 2018 FIS update. Additionally, the FIRMette has been included on Figure 4.

It should be noted that the FIS profiles and mapping (noted above) are published as feet above the North American Vertical Datum of 1988 (NAVD88), as is the effective model produced by WEST for the 2014 Nehalem River LOMR. All elevations referenced in this report and associated modeling files are based on the NAVD88 datum.



#### 2.2 PROPOSED FLOODWAY DEVELOPMENT

Trent and Kellie Davis propose to build a new deck at their property located at 16395 McDonald Dike Road in Nehalem, Oregon. The property is shown on Figure 1, the site vicinity map. The proposed deck was designed by Stricker Engineering and will extend along the south and western sides of the Davis's house. The construction plans are included in Appendix C. The entire property is located within the Nehalem River floodway, which means that any fill or development on the property must meet no-rise requirements. It must be shown that the proposed deck will not increase the 100-year base (1%-annual chance) flood elevations, floodway elevations, or floodway widths on the Nehalem River at published or unpublished cross-sections as shown on the 2018 effective FIS for Tillamook County.

The proposed deck will be located above the 100-year base flood elevation (BFE) of 16.1 feet, and therefore will not impact the 100-year flow. However, the support posts do act as obstructions that must be evaluated. As shown on the construction plans (Appendix C), a row of 6" x 6" support posts will be installed roughly 9.25 feet west of the house and a second row will be installed 13.5 feet west of the house. These rows of support posts are in a line parallel with the flow of the river, therefore each row acts as a single obstruction. A portion of the new deck will be constructed on the south side of the house; however, this will not obstruct the floodplain conveyance any further than the obstruction that the house already presents. A "no-rise" certification is required prior to construction of the deck to demonstrate no adverse impact from the proposed improvements and construction of the support posts for the deck.

#### 3.0 NO-RISE HYDRAULIC MODELING

The basic process to evaluate the no-rise performance standard uses four modeling steps as follows:

- Duplicate Effective Model: The Duplicate Effective model confirms that the effective
  model was received and reproduces published information from the FIS, or any map
  amendment studies. The Duplicate Effective model serves to validate the source of the
  Corrected Effective model (described next) but is not further used in the no-rise analysis.
- Corrected Effective Model: Changes are made to the Duplicate Effective model to create
  the Corrected Effective model. Changes may include correction of errors in the Duplicate
  Effective model, the addition of new cross-sections, or refinement of existing cross-sections
  with more detailed topographic information, to improve modeling methods and/or to allow
  future conditions to be modeled. Man-made physical changes that have occurred since the
  date of the Effective Model should not be incorporated in the Corrected Effective model.



The Corrected Effective model includes all the cross-sections that will be required to model proposed improvements with the Proposed Conditions model.

- Existing (Pre-Project) Conditions Model: Changes are made to the Corrected Effective
  Model to reflect any modifications that have occurred within the floodplain since the date of
  the Effective model. The model is identical to the Corrected Effective model if no changes
  have occurred since the date of the Effective model.
- Proposed Conditions Model: Changes to the Existing Conditions model geometry are
  made only to reflect proposed project changes. The results from this model will indicate the
  100-year elevation for the proposed conditions at the project site. These results must
  indicate no rise in the water surface elevation or floodway when compared to the Existing
  Conditions model.

For the WEST LOMR, the Nehalem River was studied from FEMA effective Cross-Section B (river station 0.45) to Cross-Section O (River station 6.8), corresponding to a length of approximately 6.35 miles (33,528 ft).

#### 3.1 DUPLICATE EFFECTIVE MODEL

Project No.: 1026

The effective hydraulic model used for the LOMR for the Lower Nehalem River was finalized in June 2014 by WEST for the Tillamook County Department of Community Development. PWR obtained the effective model for the Lower Nehalem River from WEST directly. The model includes the geometries, flow files, and floodway encroachment stations necessary for FEMA analysis.

The effective model utilized HEC-RAS Version 4.1 from the US Army Corps of Engineers (USACE). For this no-rise study, the HEC-RAS Version 4.1 model input was executed in the current standard HEC-RAS Version 6.3.1 (USACE; 2022). This HEC-RAS model constitutes the Duplicate Effective model. The Duplicate Effective model does not incorporate any changes, but simply confirms that the base model matches the output in the effective FIS. This Duplicate Effective model was then modified to create the Corrected Effective model, as described below.

The hydrology for the LOMR completed by WEST in 2014 did not modify the flows used in the prior FIS, which were developed by the U.S. Army Corps of Engineers using a hydrologic model that was calibrated to measured data at USGS stream gage 14301000, *Nehalem River near Foss*, *OR* (WEST, 2014). The flows utilized in this no-rise analysis were unchanged from the effective model. Additionally, no changes were made to the effective floodway. The encroachment stations for the new cross-sections were measured from the FIRM to maintain the effective floodway width.



#### 3.2 CORRECTED EFFECTIVE MODEL

Changes made to develop the Corrected Effective model from the Duplicate Effective model are summarized as follows:

- New cross-sections (XS 3.7542 and XS 3.7656) were added at the upstream and downstream faces of the Davis's house to add resolution and accurately model the proposed project area. The locations of the new cross-sections are shown on Figure 3.
- Lidar collected in 2009 by DOGAMI was used for the ground surface of the overbanks for
  the two new cross sections (NOAA, 2009). No changes to the ground topography near the
  Davis property is believed to have occurred since 2009, making the lidar a suitable source
  of topographic information. (Note: The 2009 lidar from DOGAMI that was used to create the
  overbank geometry for the two additional cross-sections is the same data that was used by
  WEST to create the effective cross-sections as part of their 2014 LOMR.)
- Channel bathymetry is not able to be measured using lidar. Therefore, the channel bathymetry from cross-section 3.8 was used for the two new cross-sections. The elevation of the bathymetry was adjusted based on an interpolation of the channel profile between effective model cross-sections 3.66 and 3.8. Cross-section 3.8 is located just 180 feet upstream of the Davis property. The use of bathymetry from this cross-section for the new cross-sections is reasonable given the short distance upstream and the gradually transitioning nature of the Nehalem River in this area.
- The house was added as an obstruction to cross-section 3.7656. The house existed prior to
  the date of the effective model, therefore, it is required to be added to the Corrected
  Effective model. (Note, the support posts for the existing deck were not added to the
  Corrected Effective model to be conservative with the analysis.)
- A Manning's roughness of 0.03 was assigned for the extent of the subject property at cross-section 3.7656 to represent the lawn and paved driveway between the two new cross-sections. This portion of the cross-section in the effective cross-section 3.8 has a Manning's roughness of 0.2, which was likely selected to reflect the houses (not modeled as obstructions in the effective model) and large vegetation present just upgradient of the top of the river bank. Photos of the property are included in Appendix D.
- The encroachment stations for the new cross-sections were measured from the FIRM to maintain the effective floodway width, per FEMA requirements.

Changes made were documented within the HEC-RAS model input as comments to the geometry file for the affected cross-sections. Appendix A includes a plot of the 100-year flood profile for the modeled portion of the Nehalem River, a summary of the model output, and plots of cross-sections utilized in the model (FEMA Sections B through O) for the Corrected Effective model.



#### 3.3 Existing (Pre-Project) Conditions Model

No known modifications have occurred within the study reach since the date of the Effective Model. Therefore, the Existing Conditions model is identical to the Corrected Effective model. For this reason, a separate Existing Conditions model was not created.

#### 3.4 Proposed Conditions Model

Changes made to model the proposed project are summarized as follows:

 The proposed support posts for the deck were modeled as obstructions and added to cross-section 3.7656. Two obstructions were added to this cross-section, as there are two rows of support posts perpendicular to the direction of flow of the river.

As with the Corrected Effective model, changes made were documented within the HEC-RAS model input as comments to the geometry file for the affected cross-sections. Appendix B includes a plot of the 100-year flood profile for the modeled portion of the Nehalem River, a summary of the model output, and plots of cross-sections utilized in the model (FEMA Cross-Sections B through O) for the Proposed Conditions model.

#### 3.5 No-RISE RESULTS

Table 1 compares the base flood elevations for the Proposed Conditions model with those for the Corrected Effective/Pre-Project model. As described previously, no changes were necessary for the Pre-Project model; therefore, the Corrected Effective model represents both scenarios. The 100-year Proposed Conditions model resulted in a 0.01-foot decline at cross-section 5.951. At all other locations, the difference in water surface elevations was 0.00 feet. No rise was observed at any cross-section in the analysis of the Nehalem River as a result of the proposed deck construction.

Cascade Water Resources, LLC

March 6, 2023 Page 5



#### 4.0 CONCLUSIONS

Based on the detailed analysis described above, construction of the proposed deck at the property located at 16395 McDonald Dike Road meets the requirements for a no-rise finding if constructed as described in the construction plan set included in Appendix C.

We appreciate this opportunity to be of service. Please feel free to contact me if you have any questions regarding this report.

Sincerely,

Roger Sutherland, PE

Cascade Water Resources, LLC

R.C. Smit

#### No-Rise Report for Nehalem River at McDonald Dike Road Nehalem, Oregon



#### REFERENCES

FEMA, 2018. Flood Insurance Study and Map Panel 41057C0230F for Tillamook County, Oregon (41057CV001A). Federal Emergency Management Agency, Washington, DC. Effective September 28, 2018.

NOAA, 2009. National Oceanic and Atmospheric Administration (NOAA) Digital Coast Data Access Viewer. Custom processing of "2009 OR DOGAMI Lidar: North Coast". Charleston, South Carolina. Data accessed October 30, 2022, at https://coast.noaa.gov/dataviewer.

USACE, 2022. HEC-RAS Program Version 6.3.1. US Army Corps of Engineers Hydraulic Engineering Center. Davis, CA. September 2022.

WEST, 2014. LOMR Submittal: Lower Nehalem River – Tillamook County, Oregon. WEST Consultants, Inc. Portland, OR. June 2014.

#### No-Rise Report for Nehalem River at McDonald Dike Road Nehalem, Oregon



#### LIMITATIONS

This report was prepared exclusively for Trent and Kellie Davis by Cascade Water Resources, LLC (CWR). The quality of information, conclusions, and estimates contained herein is consistent with the level of effort involved in CWR services and based on: i) information available at the time of preparation, ii) data supplied by outside sources, and iii) the assumptions, conditions, and qualifications set forth in this report. This no-rise report and certification is intended to be used by Trent and Kellie Davis for their property located at 16395 McDonald Dike Road in Nehalem, Oregon only, subject to the terms and conditions of its contract with CWR. Any other use of, or reliance on, this report by any third party is at that party's sole risk.

Table 1
No-Rise Modeling Results

	Corrected Effe	ective/Pre-Project	Propose	ed Condition	
Flow (cfs)	Cross Section <sup>1</sup>	BFE (ft NAVD88) <sup>2</sup>	Cross Section <sup>1</sup>	BFE (ft NAVD88) <sup>2</sup>	Change in BFE (ft) <sup>3</sup>
59,000	6.8	24.09	6.8	24.09	0
.59,000 4	6.61 s	21.2	6.61	21,2	0
59,000	6.584	21.3	6.584	21.3	0
59,000	6.583	21.17	6.583	21.17	0
59,000	6.579	21.15	6.579	21.15	0
59,000	6.578	21.16	6.578	21.16	0
59,000	6.559	20.98	6.559	20.98	0
59,000	6.25	20.33	6.25	20.33	0
56,700	6.01	18.23	6.01	18.23	
Bridge	5.99		5.99		
54,700	5.98	18.06	5.98	18,06	0
54,700	5.951	18.01	5.951	18	-0.01
54,700	5.88	18.11	5.88	18.11	0
54,700	5.79	17.89	5.79	17.89	0
54,700	5.65	17.53	5.65	17.53	0
54,700	5.55	17.58	5.55	17.58	0
54,700	5.34	17.69	5.34	17.69	0
54,700	5.26	17.66	5.26	17.66	0
54,700	5.17	17.64	5.17	17.64	.0
54,700	4.78	17.56	4.78	17.56	0
54,700	3.8	16.03	3.8	16.03	0
54,700	3.7656	16.15	3.7656	16.15	0
54,700	3.7542	16.06	3.7542	16.06	0
52,600	3.66	16.22	3.66	16.22	Ö
52,600	3.28	15.79	3.28	15.79	0
52,600	3.24	15.75	3.24	15.75	0
52,600	3.12	15.68	3.12	Part of the second	0
52,900	2.92	15.53	2.92	15.53	0
52,900	2.49	15.15	2.49	15.15	0
52,900	2.28	14.95	2.28	14.95	0
66,400	2.01	14.84	2.01	14.84	0
66,400	1.92	14.74	1.92	14.74	0
66,400	1.74	14.31	1.74	14.31	0
66,400	1.5	14.04	1.5	14.04	0
66,400	1.33	13.88	1.33	13.88	0
66,700	1.05	10.7	1.05	13.7	0
67,000	0.994	13.68	0.994	13.68	0
67,000	0.95	13.63	0.95	13.63	0
Bridge	0.92		0.92		
67,000	0.86	13.55	0.86	13.55	0
67,000	0.8	13.5	0.8	13.5	0
67,000	0.78	13.4	0.78	13.4	0
67,000	0,73	13,36	0.73	13.36	0:
67,000	0.6	13.32	0.6	13.32	0
74,000	0.45	13.11	0.45	13.11	0

#### Notes

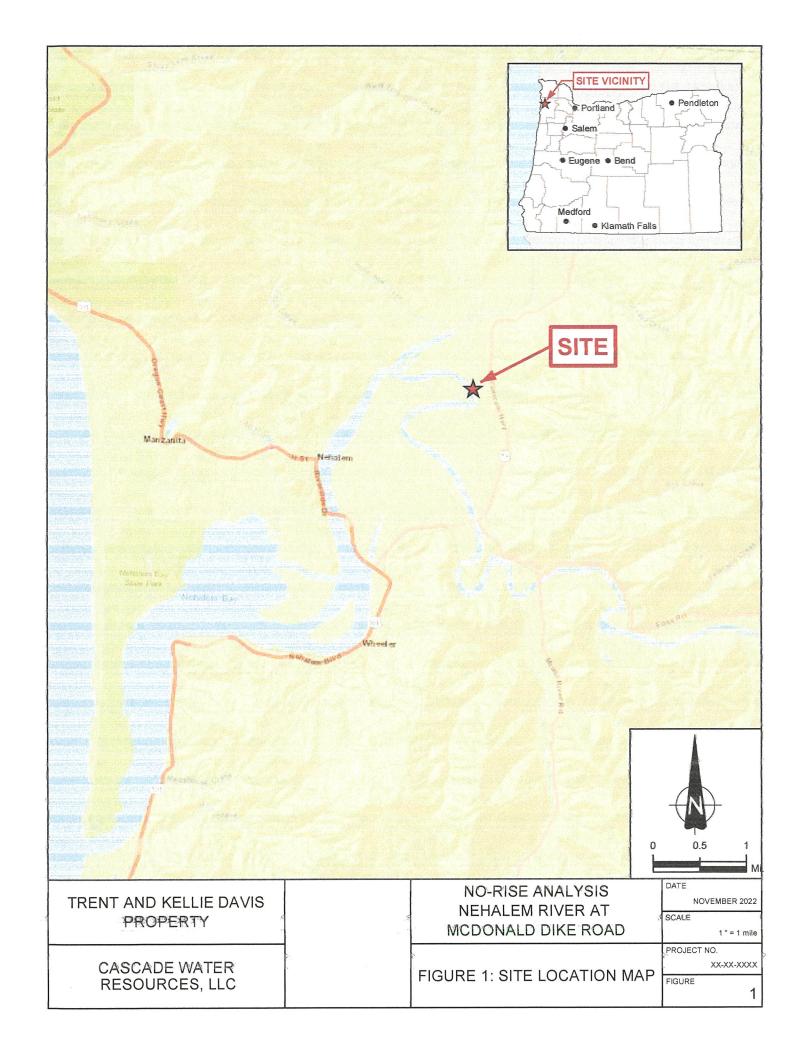
#### Abbreviations:

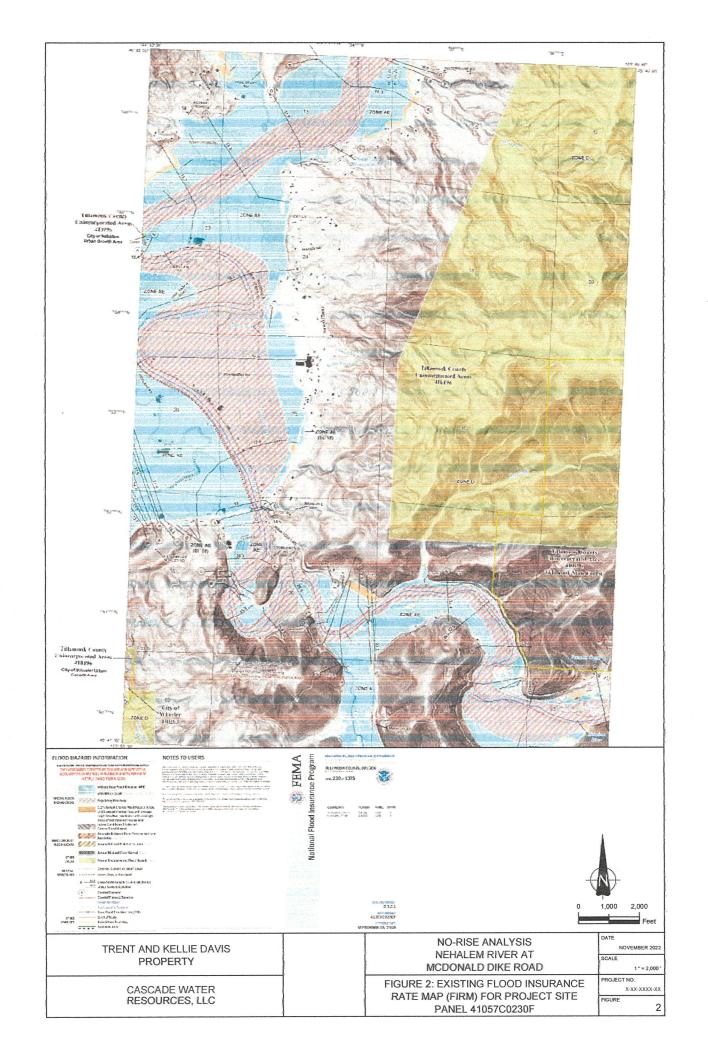
BFE - Base Flood Elevation, the regulatory (100-year) flood water surface elevation

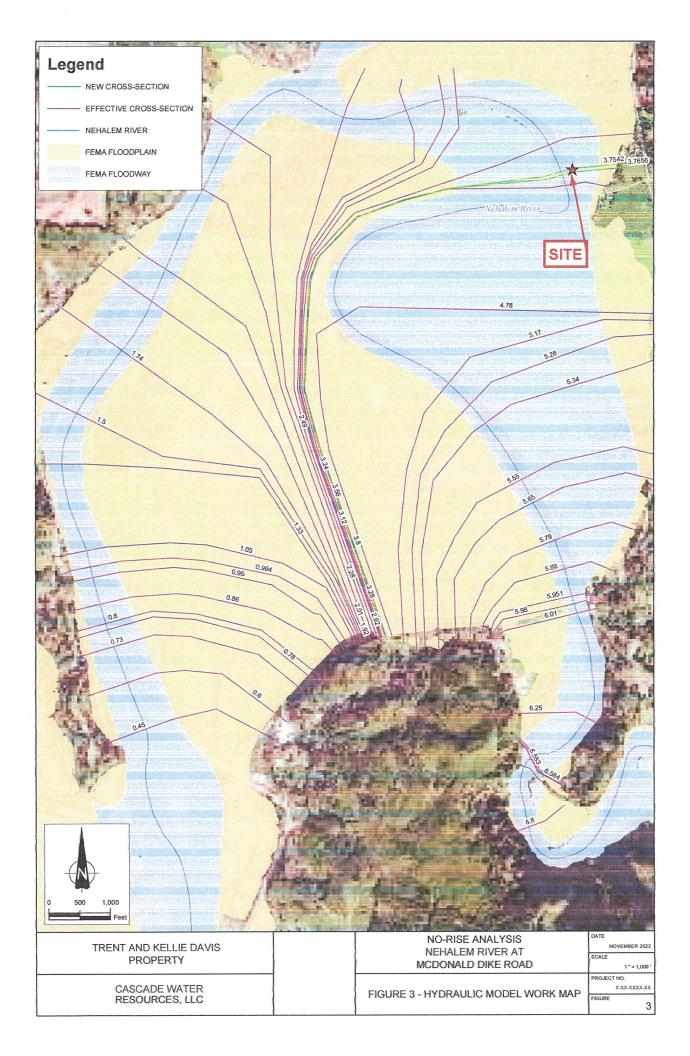
<sup>&</sup>lt;sup>1</sup> Cross Section No. is the distance in miles upstream from the end of the effective model.

 $<sup>^{2}\,\</sup>mathrm{All}$  model elevations are in North American Vertical Datum of 1988 (NAVD88).

<sup>&</sup>lt;sup>3</sup> Change in water surface elevation is calculated as the difference between the Corrected Effective / Pre-Project Conditions Model and the Proposed Conditions Model.

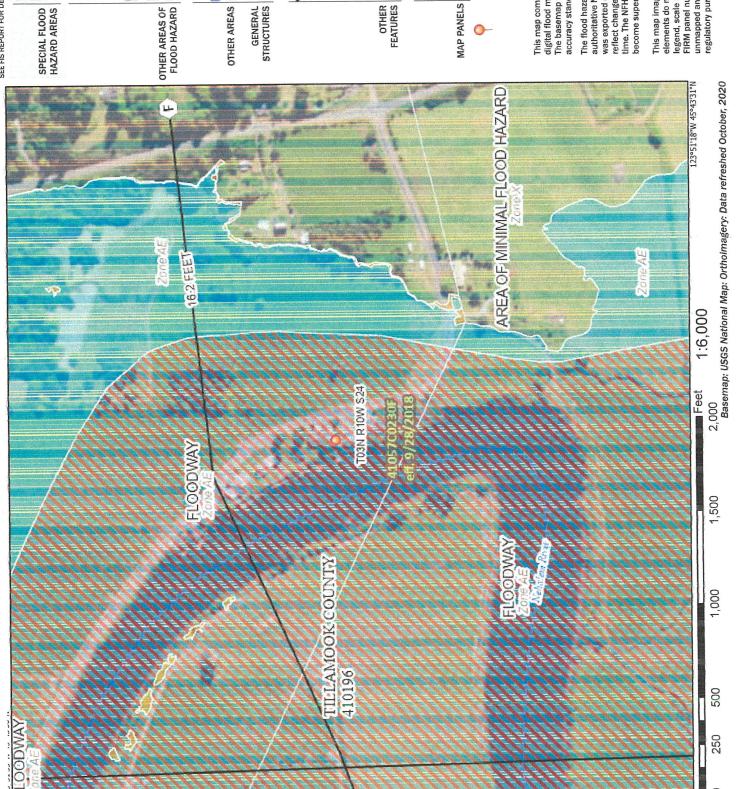






# Figure 4 - FEMA FIRMette





## Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

Without Base Flood Elevation (BFE)

Zone A, V, A99 With BFE or Depth Zone AE, AO, AH, VE, AR Regulatory Floodway 0.2% Annual Chance Flood Hazard, Areas of 1.% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X Area with Reduced Flood Risk due to Future Conditions 1% Annual Chance Flood Hazard Zone

Area with Flood Risk due to Levee Zone D Levee. See Notes. Zone X

No screen Area of Minimal Flood Hazard Zone **Effective LOMRs** 

Area of Undetermined Flood Hazard Zone D

Channel, Culvert, or Storm Sewer GENERAL ----- Channel, Culvert, or Storn STRUCTURES | 11111111 Levee, Dike, or Floodwall

Cross Sections with 1% Annual Chance Water Surface Elevation 17.5

Base Flood Elevation Line (BFE) Coastal Transect Limit of Study

Jurisdiction Boundary

Coastal Transect Baseline Hydrographic Feature Profile Baseline

OTHER

Digital Data Available

No Digital Data Available Unmapped The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map compiles with FEMA's standards for the use of digital flood maps if it is not vold as described below. The basemap shown compiles with FEMA's basemap

authoritative NFHL web services provided by FEMA. This map reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or The flood hazard information is derived directly from the was exported on 9/27/2021 at 4:11 PM and does not become superseded by new data over time. This map image is vold if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, FIRM panel number, and FIRM effective date. Map images for egend, scale bar, map creation date, community identifiers, unmapped and unmodernized areas cannot be used for regulatory purposes.

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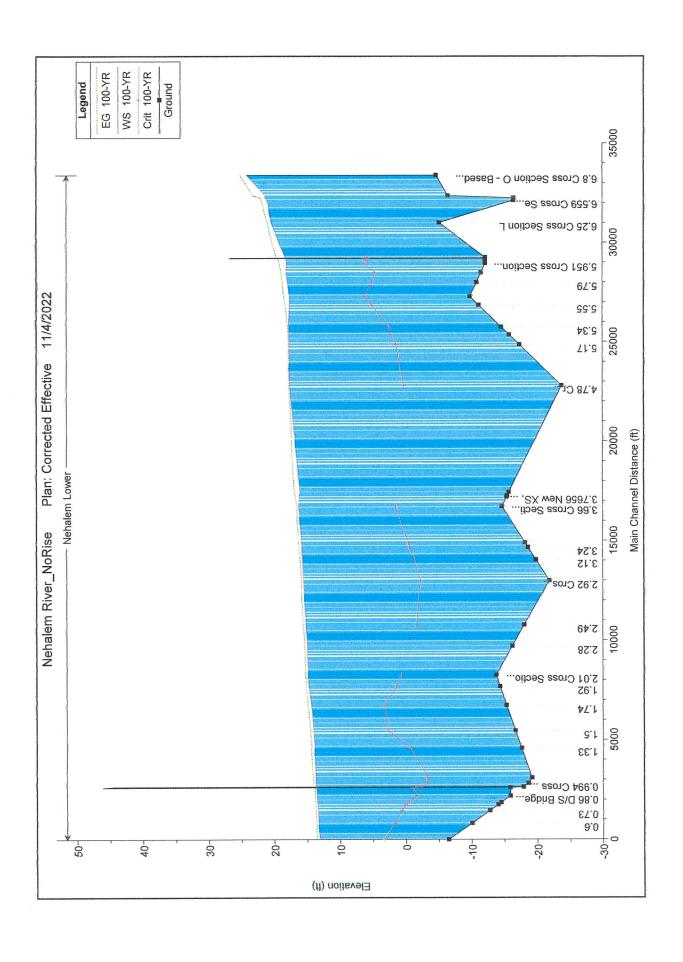
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Corrected Effective / Pre-Project Conditions Hydraulic Model Output

Profile

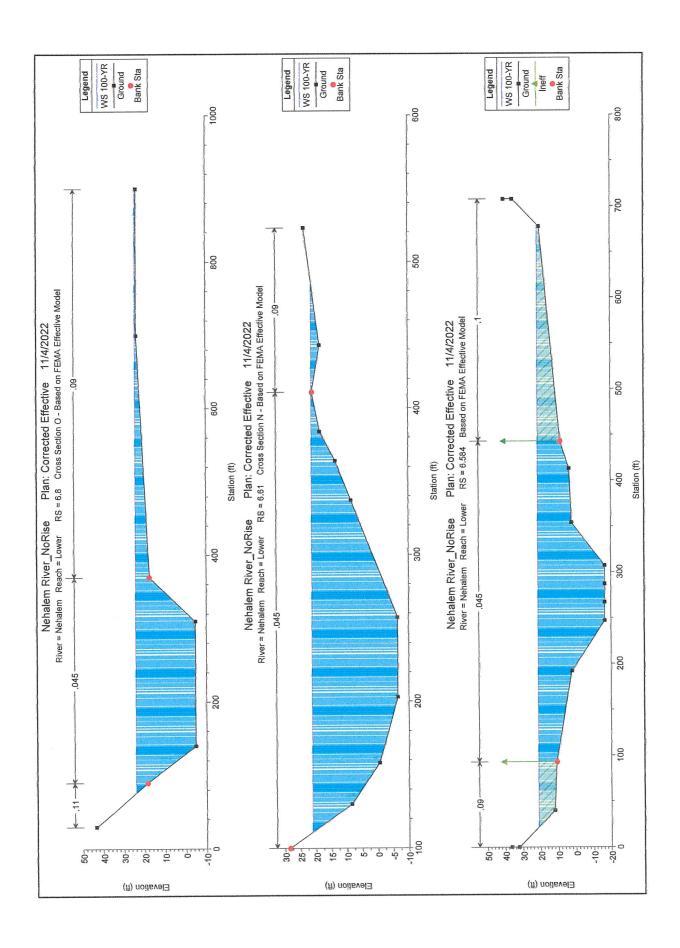
**Output Summary** 

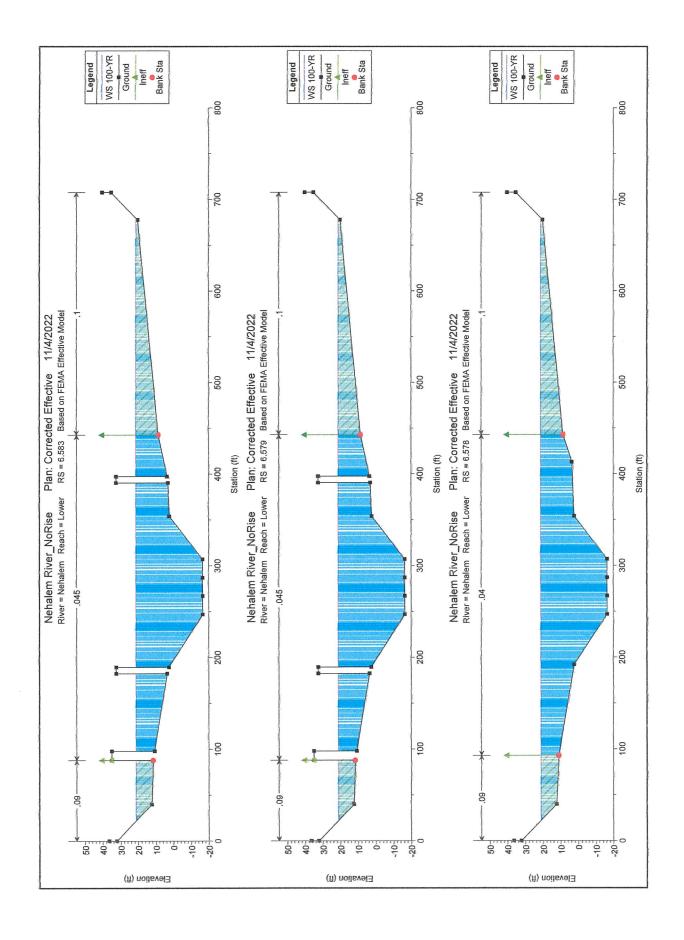
Cross-Sections

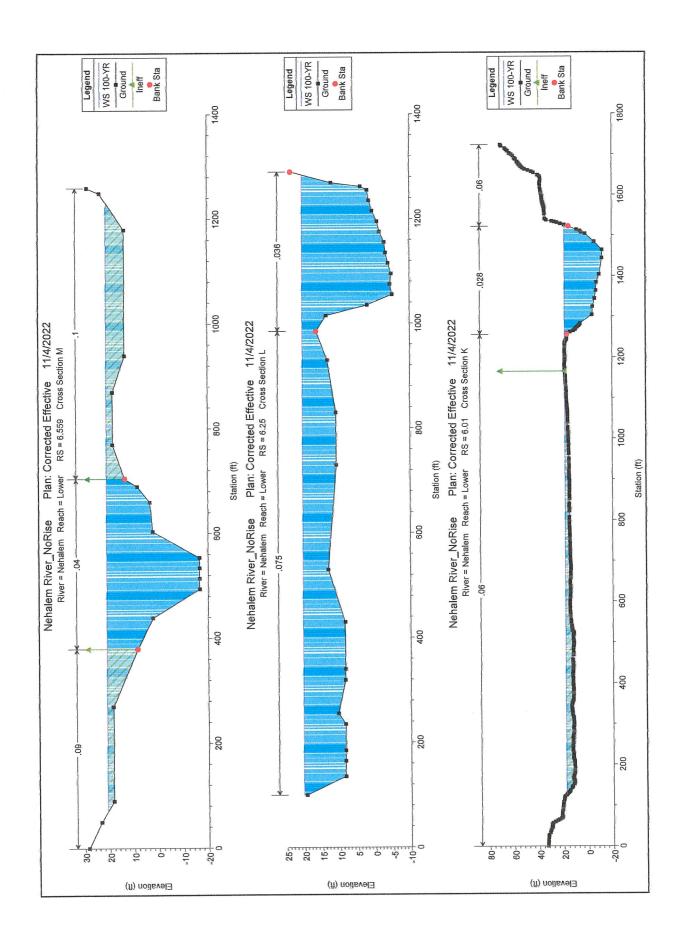


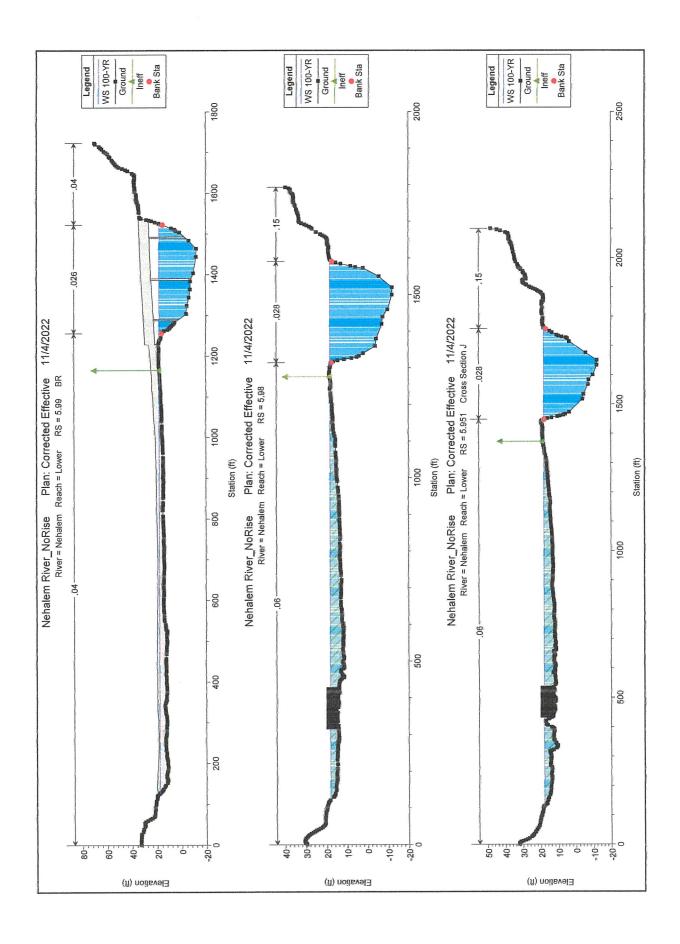
	wer Profile: 100-YR
	Reach: Lower
	HEC-RAS Plan: Corr_Eff River: Nehalem
	Plan: Corr_Eff
	HEC-RAS Pla

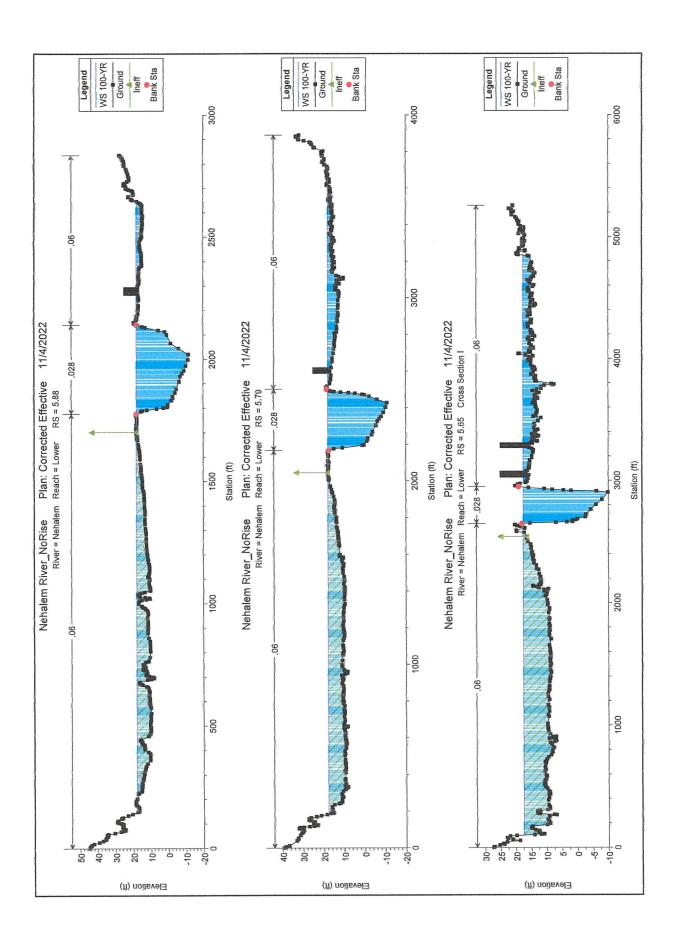
River Sta	Profile	O Total	Min Ch El	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	Vel Chnl	Flow Area	Top Width	Froude # Chl
		(cfs)	( <b>y</b> )	( <b>u</b> )	( <b>u</b> )	æ	(11/11)	(s/tj.)	(sq ft)	( <b>u</b> )	
	100-YR	59000.00	-4,66	24.09		25.19	0.000981	8.49	8120.93	823.32	0:30
	100-YR	59000.00	-8,46	21.20		23.17	0.002661	ر 11.25	5335.85	374.63	0.47
	100-YR	59000.00	-15,46	21.30		22.12	0.000745	7.24	8146.01	657.94	0.26
	100-YR	59000.00	-18,46	21.17		22.07	0.001092	7.61	7751.26	7	0.28
	100-YR	59000.00	-15,46	21.15		22.05	0.001095	7.62	7743.80	633.34	0.28
	100-YR	59000.00	-16,46	21.16	2	21.99	0.000600	7.29	8098.21	657.40	0.27
	100-YR	59000.00	-16,46			21.88	0.000642	7.65	7713.58	1161.53	0.28
	100-YR	59000.00	5.16	20.33		20.91	0.000643	7.22	13893.07	1184.08	0.29
	100-YR	56700.00	1,2,16	18.23	5.84	19.63	0.000538	9.49	5999.65	1340.73	0.35
		Bridge	8					۶			
	100-YR	54700.00	12,16	18.06		19.25	0.000456	72.8	6245.01	1318.92	0.33
	100±YR	54700.00	-12.16	18.01	6,21	19.19	0.000507	8.72	6275.78	1429.68	0.34
	100-YR	54700.00	11,52	18.11	4.60		0,000319	2.06	8623.08	2389.05	0.27
	100-3/R	54700.00	10.84	17.89		18.70	0.000361	7.46	10112.08	3409.98	0.29
	100-YR	54700.00	-9.86	17.53		18.41	0.000437	66.7	11569.08	4657.89	0.31
	100-YR	54700.00	211.18	17.58	5.07	18.18	0.000284	0.70	14758.91	5541.33	0.26
	100-VR	54700.00	14,61	17.69	2,53	17.87	0.000102	4.31	27737.78	6611.34	0.16
	100-Y.R	54700.00	15,84	17.66	2.23	17.83	0.000098	4.22	29537.28	7050.75	0.15
	100-YR	54700.00	17,37	17.64	1.38	17.77	0.000085	4.00	33451.00	7419.27	0.14
	100-¥R	54700.00	-23.76	17.56	0.30	17.66	0.000071	3.63	41857.13	10506.49	0.13
	100-YR	54700.00	-15,74	16.03		16.94	0.000417	8.22	13127.95	10640.01	0.31
3.7656	100-YR	54700.00	-15,48	16.15		16.80	0.000332	7.32	16289.90	10807.45	0.28
3.7542	100-YR	54700.00	÷15,39			16.78		Ş	- {	¥10909.10	0.29
	100-YR	52600.00	≥14,66	16.22	1.47	16.56		:54			0.20
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	100-YR	52600.00	-18,62	15.75	-0.56	16.19	0.000178	5.78		10082.66	0.21
	100-YR	52600,00	19,83		-1,27	16.08	0.000162	5.45		9947.19	0.20
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	100-YR	66400.00	-15.36					- 1		3	0.26
	100-YR	66400,00	-16,69	14.04	2,57	14.54	0.000250	6.10	13180.32	7425.06	0.26
	100-分配	66400.00	17,61		-0.79	14.35	0.000162	5.55	12351.71	6337.32	0.21
	100-YR	00'00'99	-19.16	13.70	-3.17	14.12	0.000135	5.20		5319.91	0.19
	100-YR	00'00029	-18,66	13.68	-3.15	14.06	0.000131	4.96		4996.52	0.19
	100-YR	67000.00	-17,89	13.63	-2.40	14.03	0.000142	5.09	13390.30	4808.98	0.20
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	100-YR	00'00029			-1.63	13.87		3		Ž.	0.19
	100-YR	00'00029			-0.51	13.82				2	0.19
	100-YR	00'00029	×14,02	. :	0.06	13.80				31.	0.21
	100-YR	00'00029	-12.75		0.59	13.75		5.06		> -	
	100-YR	00'00029	-10.00	13.32	1.72	13.63	0.000147	4.49	15373,60	2975.78	0.19
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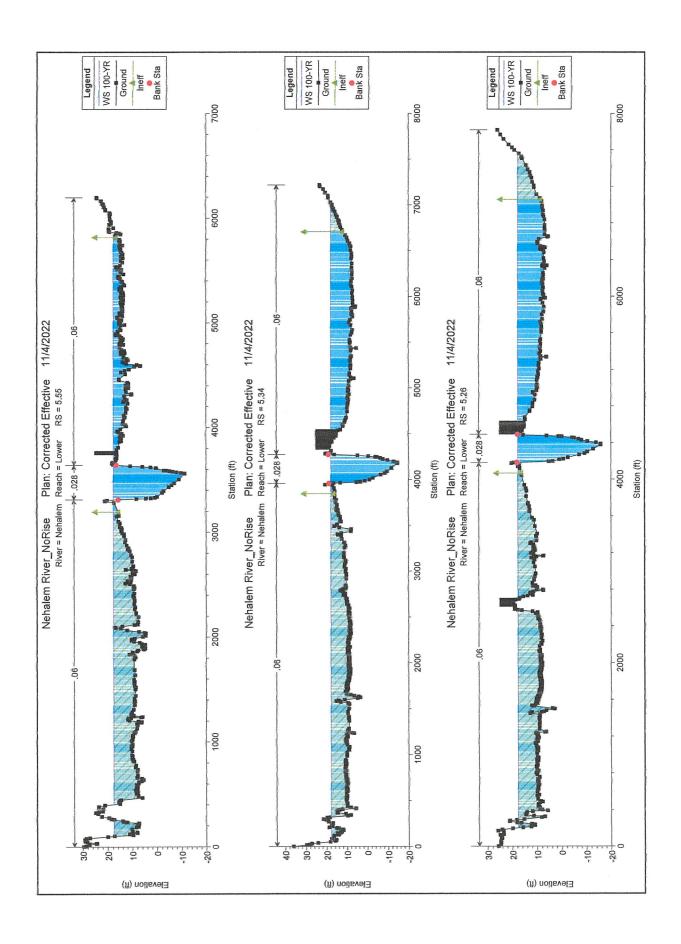


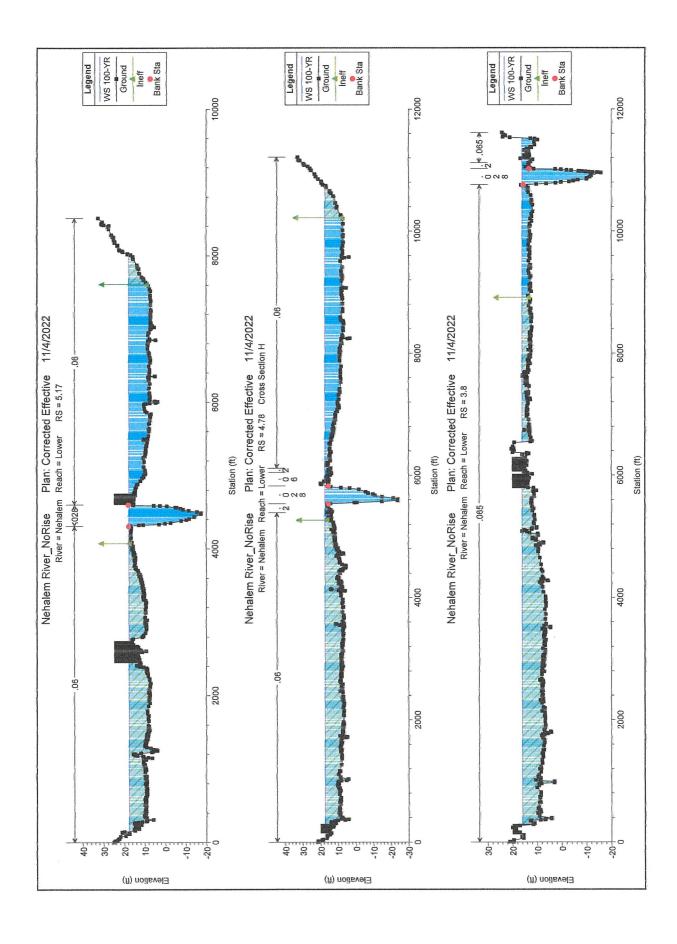


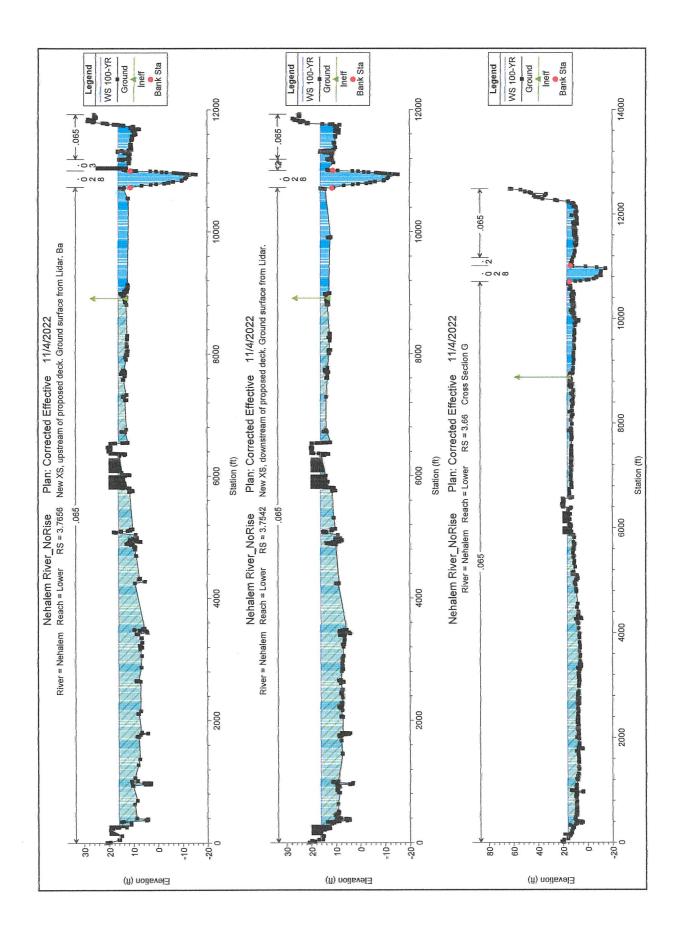


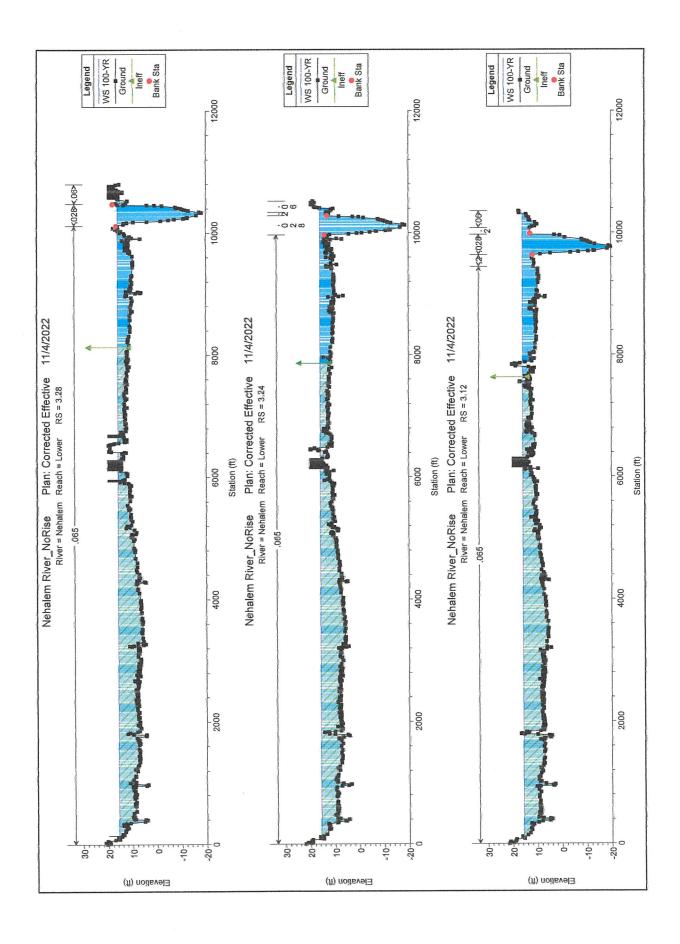


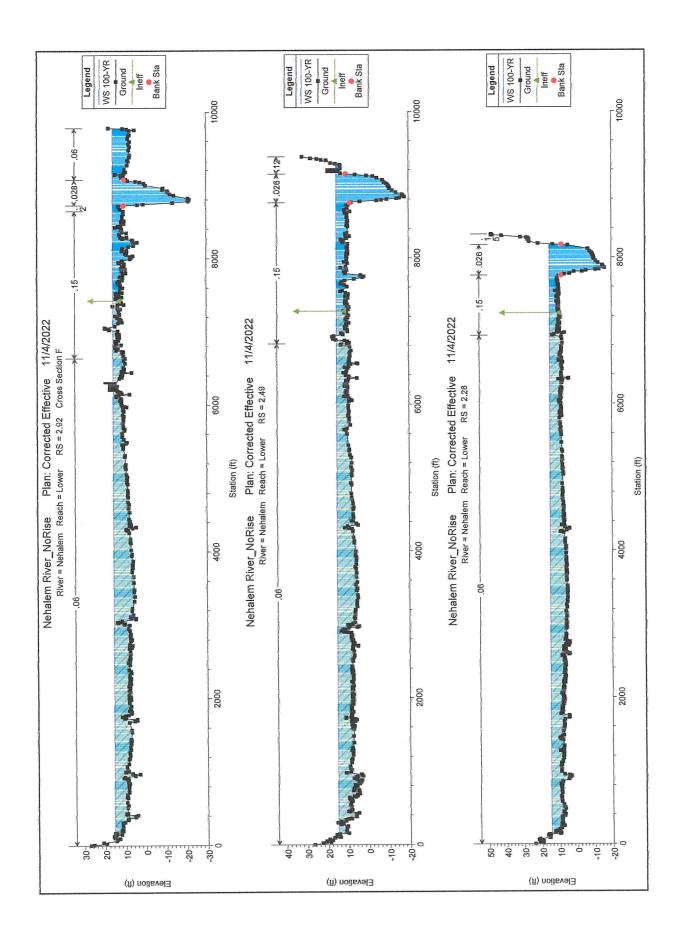


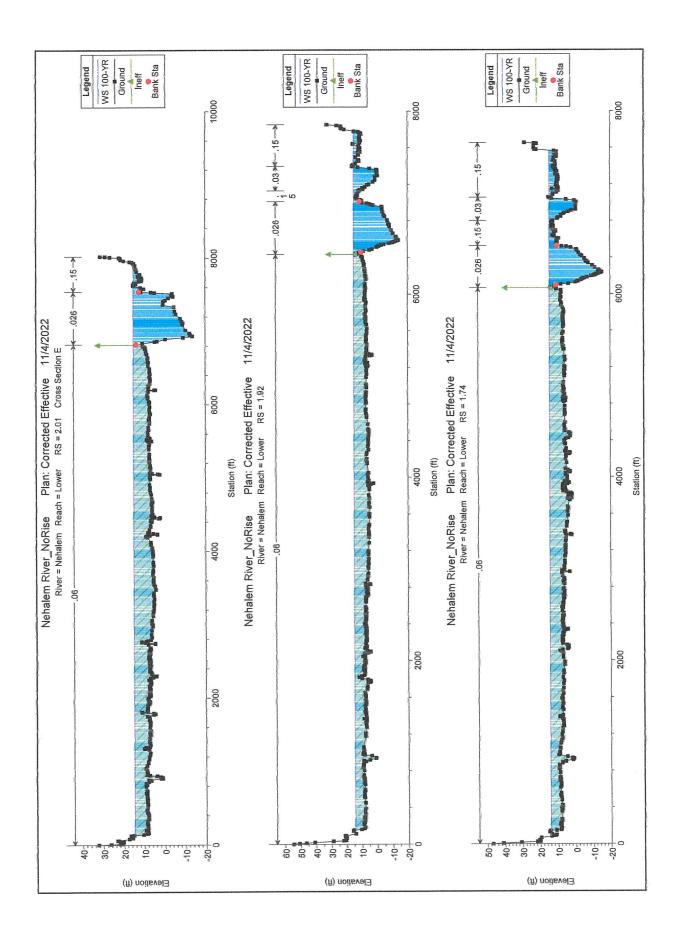


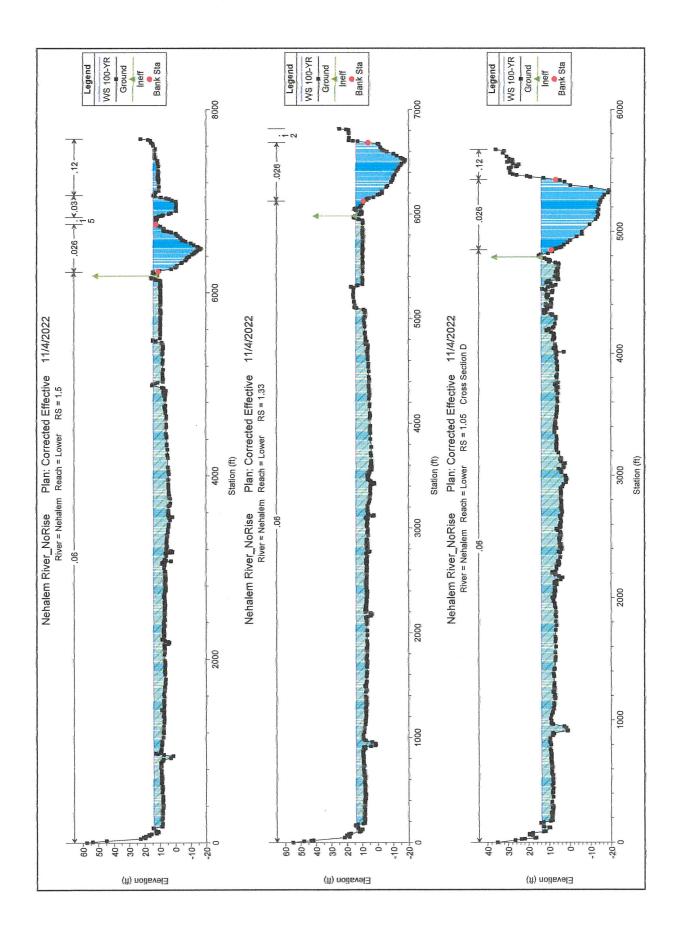


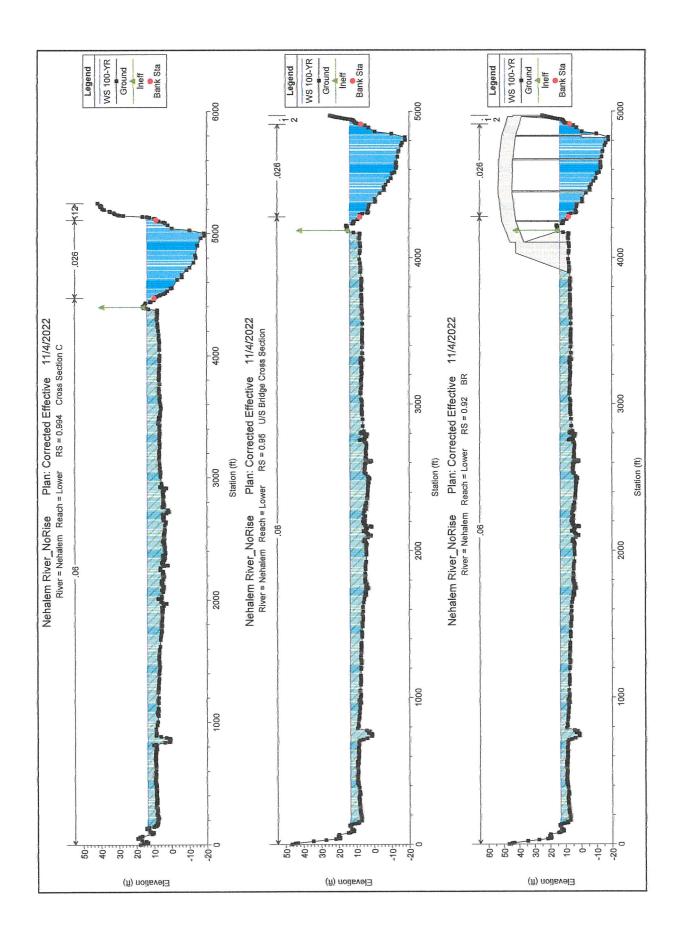


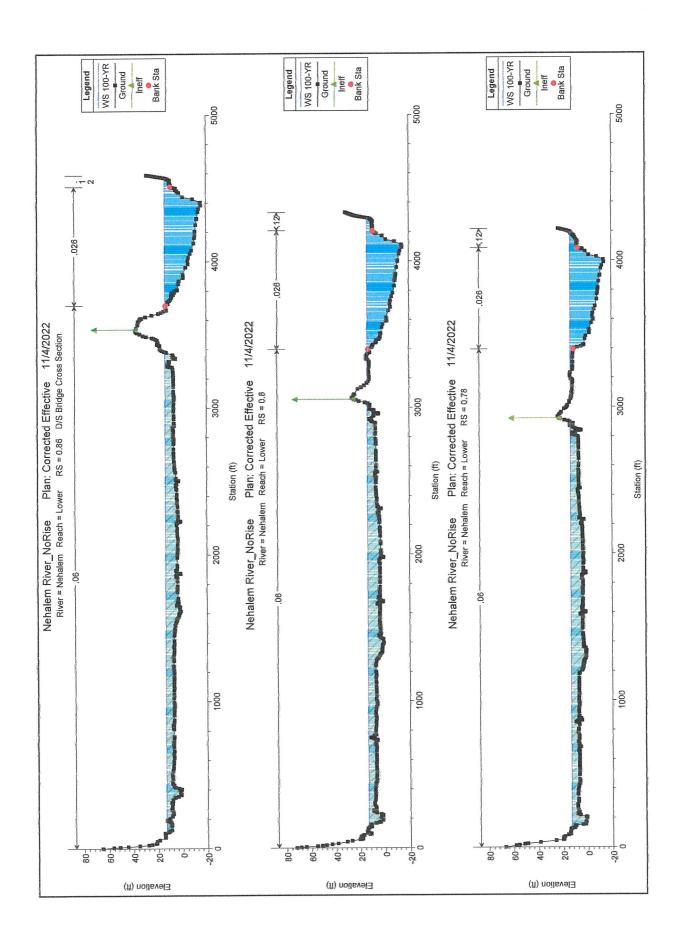


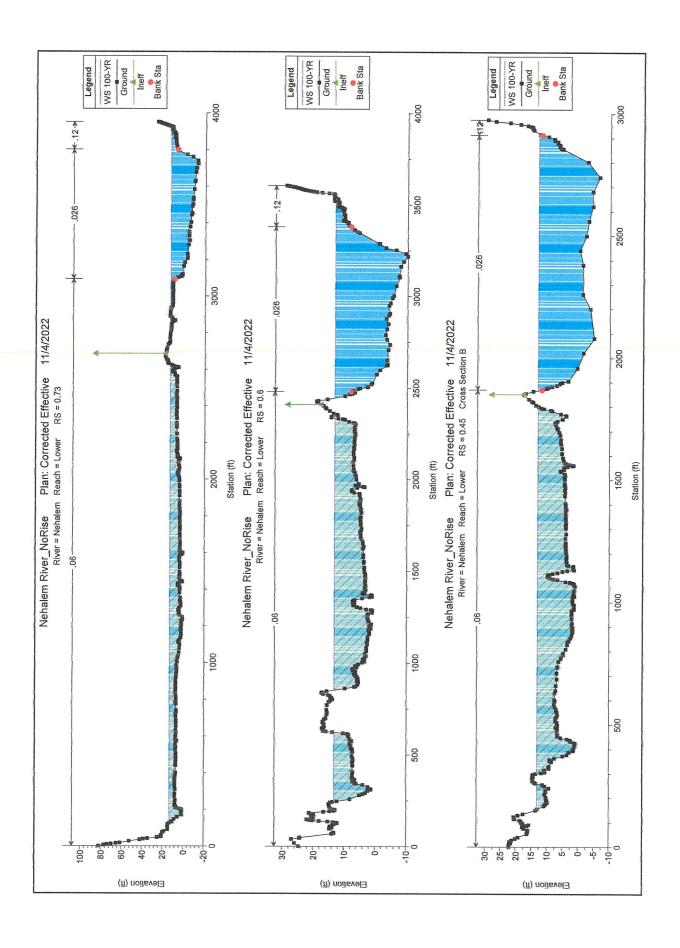












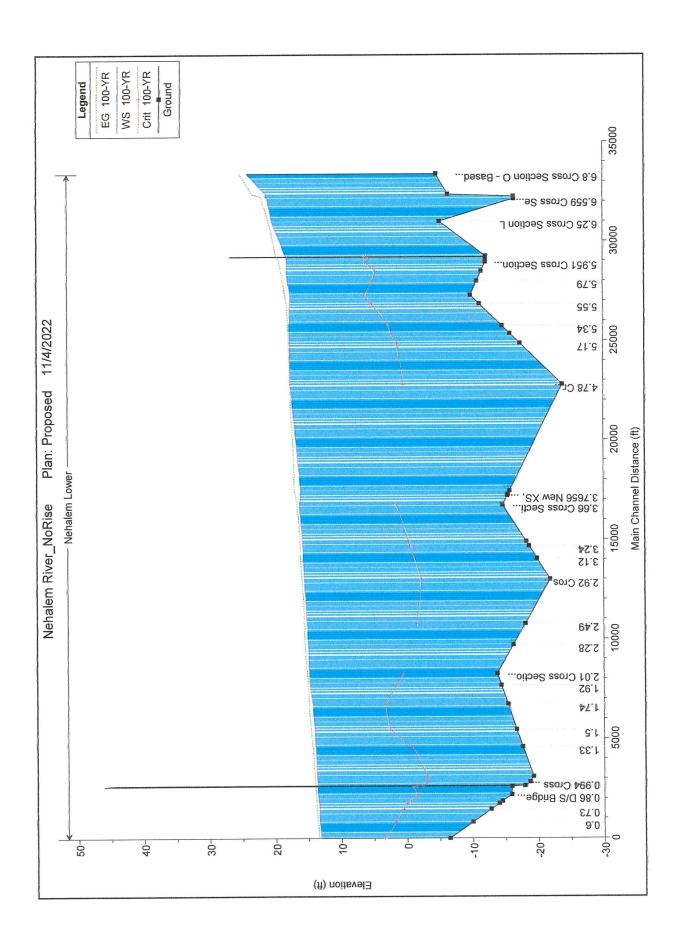
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Proposed Conditions Hydraulic Model Output

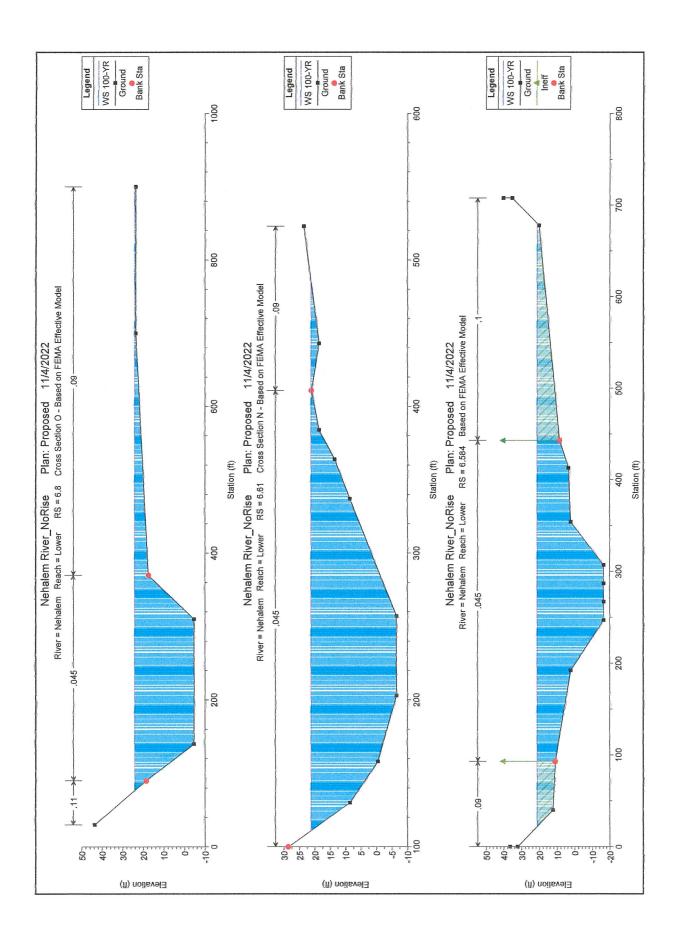
Profile

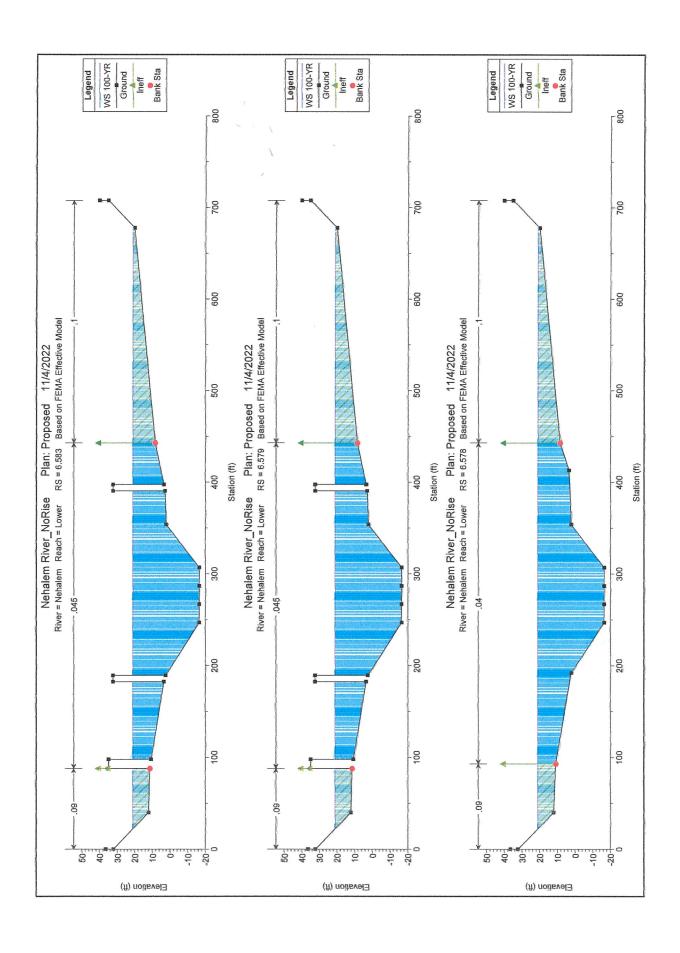
Output Summary

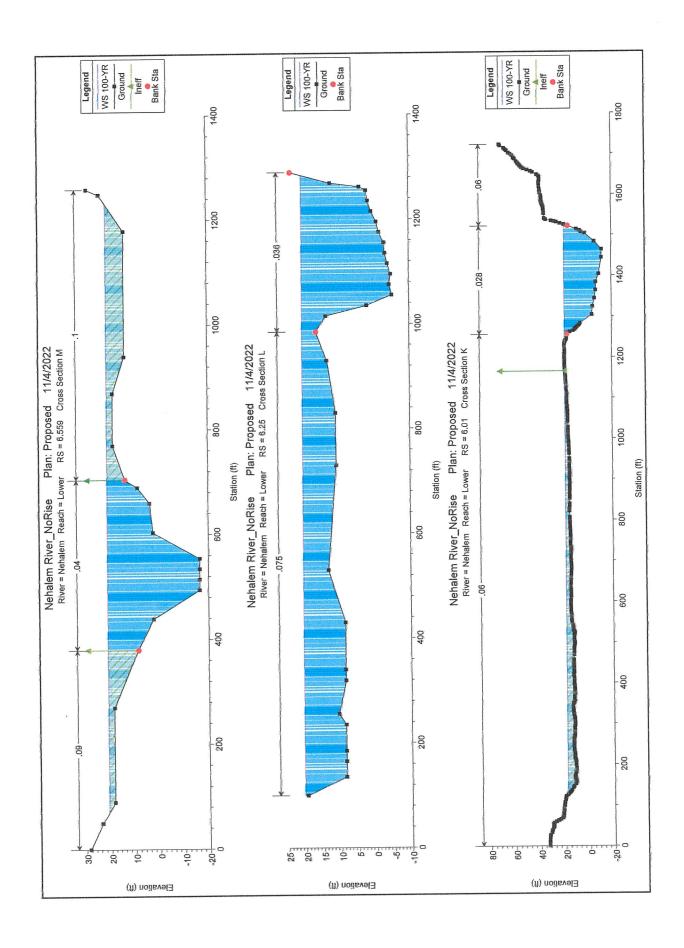
Cross-Sections

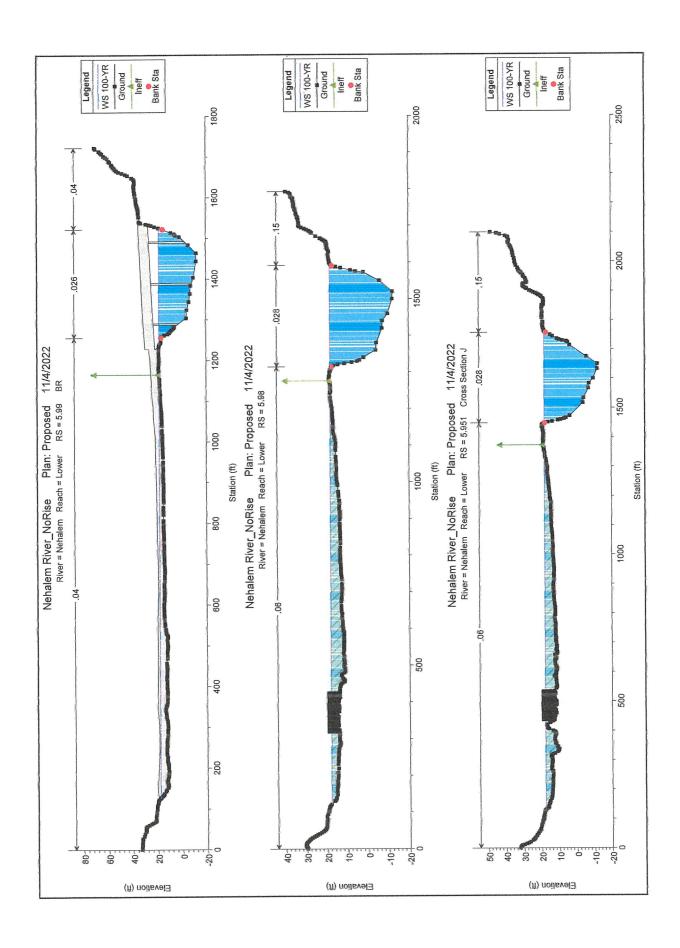


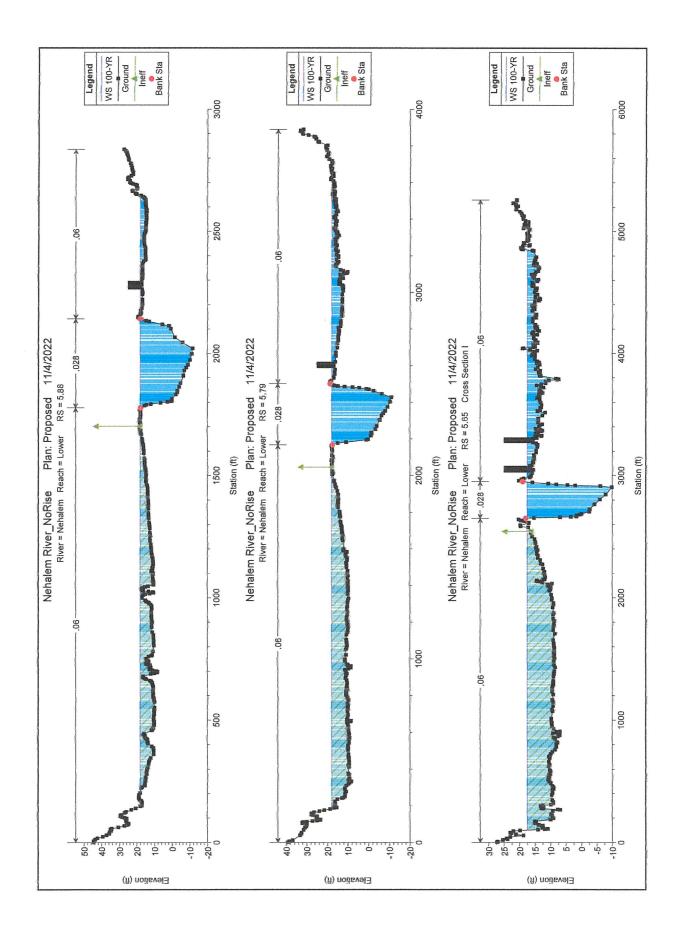
Reach	River Sta	Profile	Q Total	Min Ch.E.	W.S. Elev	Crit W.S.	E.G. Elev	E.G. Slope	VelChn	Flow Area	Top Width	Froude # Chl
			(cfs)	€	(E)	€	2	(ft/ft)	(ff/s)	(sq.ft)	(H)	
Lower	6.8	100-YR	59000.00	4.66	24.09		25.19	0.000981	8.49	8120.84	823.32	0.30
OWE	6.61	100-YR	59000.00	6.46	21.20		23.17		11.25	5335.78	374.63	0.47
Lower	6.584	100-YR	59000.00	-16.46	21.30		22.12		7.24	8145.95	5	0.26
Lower	6.583	100±YR	59000.00	-16.46	21.17	1 15	22.07	0.001092	7.61	7751.20	633.43	0.28
Lower	6.579	100-YR	59000.00	-16.46	21.15	5	22.05	0.001095	7.62	7743.74	3	0.28
Lower	6.578	10¢YR	59000,00	-18.46	21.16		21.99	0.000600	7.29	8098.15	657.40	0.27
Lower	6.559	100×YR	59000.00	-18.46	20.98		21.88	0.000642	7.65	7713.52	1161.53	0.28
Lower	6.25	100-YR	59000,00	£.16	20.33		20.91	0.000643	7.22	13892.81	1184.08	0.29
Lower	6.01	100-YR	56700.00	-12.16	18.23	5.84	19.63	0.000538	9.50	5989.57	1340.51	0.35
Lawer	5.99		Bridge	,					*		A	
Lower	5.98	100-YR	54700.00	-12.16	18.06		19.25	0.000456	8.77	6244.93	1318.88	0.33
Lower	5,951	100°YR	54700.00	-12.16	18.00	6.21	19.19		8.72	6275.69		0.34
Lower	5.88	100-YR	54700.00	-11.52	18.11	4,60	18.88	0.000320	7.06	8622.83	2388.97	0.27
Lower	5,79	100-YR	54700.00	-10.84	17.89	5,03	18.70	0.000361	7.46	10111.57	3409.91	0.29
Lower	5.65	100-YR	54700.00	-9.86	17.53	6.25	18.41	0.000437	7.99	11568.22	4657.80	0.31
ower	5.55	100-YR	54700.00	-11.18	17.58	5.07	18.18	0.000284	6.70	14757.94	5541.31	0.26
ower	5.34	100-YR	54700.00	-14.61	17.69	2,53	17.87	0.000102	4.31	27736.84	6611.26	0.16
, ower	5.26	100-YR	54700.00	15.84	17.86	2.23	17.83	0.000098	4.22	29536.22	7050.74	0.15
Loyver	5,17	100-YR	54700.00	-17.37	17.64	1.38	17.77	0.000085	4.00	33449.73	7419.24	0.14
Lower	4.78	100-YR	54700.00	-23.76	17.56	0.30	17.66	0.000071	3.63	41855.25	10506.47	0.13
Lower	3.8	100-YR	54700.00	-15.74	16.03	3	16.94	0.000417	8.22	13126.32	10639.93	0.31
Lower	3.7656	100-YR	54700.00	-15.48	16.15		16.80	0.000333	7.32	16281.59	10806.40	0.28
Lower	3,7542	100-YR	54700.00	-15.39	16.06		16.78		7.55	15683.24	10909.10	0.29
Lower	3.66	100-YR	52600.00	-14.66	16.22	1.47			5.42	23223.57	11590.21	0.20
Lower	3.28	100-YR	52600.00	÷18.19	15.79	-0,38	16.23		5.87	17036.40	9955.88	0.22
Lower	3.24	100-YR	52600.00	-1B.62	15.75	-0.56	16.19		5.78	17935.52	10082.66	0.21
Lower	3.12	100-YR	52600.00	±19.83	15.88	-1,27	16.08	0.000162	5.45	18725.99	9947.19	0.20
Lower	2.92	100-YR	52900,00	-21.86	15.53	-2.28	15.91		5.30		9515.87	0.19
Lower	2.49	100-YR	52900,00	-18.06	15.15	-1.60			5.39		9030.33	0.19
Lawer	2.28	100-YR	52900.00	+16,24	14.95				5.57		8050.01	0.21
Lower	2.01	100-YR	66400.00	-13,76	14.84	0.65			4.68		7786.01	0.19
<b>л</b> емот	1.92	100-YR	66400.00	-14.37	14.74	1,50 180		0.000151	5.15	15560.50	7606.61	0.20
Loyver	1,74	100-YR	66400.00	-15.36	14.31	3,28			6.64	13656.08	7451.94	0.26
Tower	1.5	100-YR	66400.00	-16.69	14.04	2:57			6.10	13180.32	7425.06	0.26
Lower	1.33	100-YR	66400.00	+17.61	13.88	-0.78			5.55		6337.32	0.21
ower	1.05	100-YR	66700.00	-19.16	13.70	-3.17			5.20		5319.91	0.19
Lawer	0.994	100-YR	67000.00	-18.66	13.68	-3.15	14.06	0.000131	4.96	13691.29	4996.52	0.19
Lower	0.95	100-YR	67000.00	-17.89	13.83	-2.40	14.03	0.000142	5.09	13390.30	4808.98	0.20
ower	0.92		Bridge	ŀ				î			Xee	
Lawer	0.86	100-YR	67000.00	-15.91	13.55	-1.63	13.87		4.52	15040.76	4184.05	0.19
Lower	8.0	100-YR	67000.00	-14.49	13.50	-0.51			4.59	15109.85	Á	0.19
Lawer	0.78	100-YR	67000.00	14.02	13.40	0.06			5.07		, \$	0.21
ower	6.73	100-YR	67000.00	-12,75	13.36	0.59		0.000160	5.06		3594.73	0.21
- DWer	0.6	100-YR	67000.00	-10.00	13.32	1.72			4.49		2975.78	0.19
Jewe	0.45	æ, 55-}	74000.00	A 46	13.11	200	13.48	202000	4 89	15150 11	2656 06	0.03

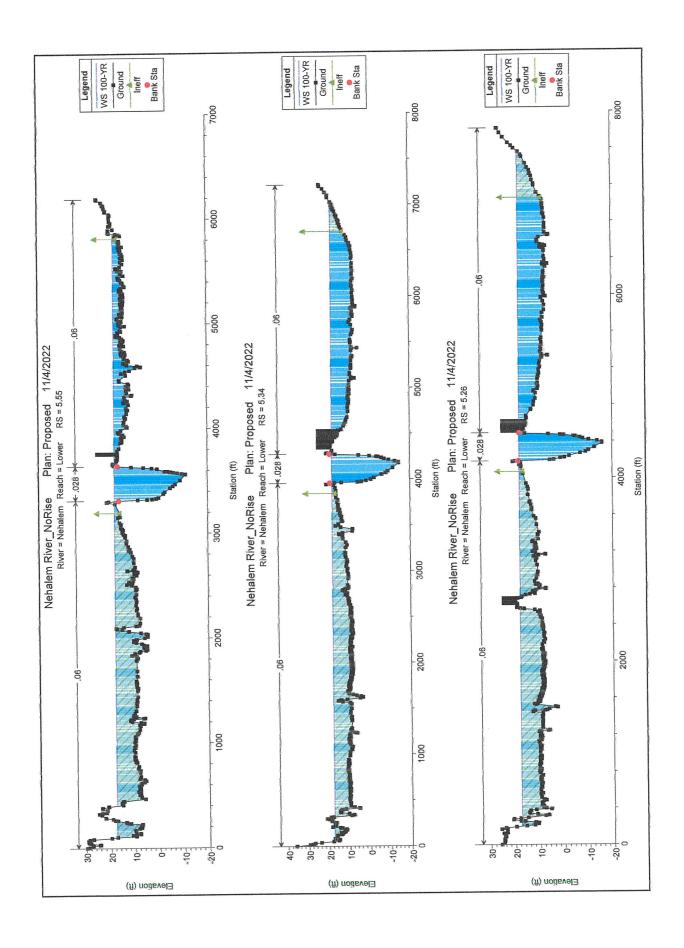


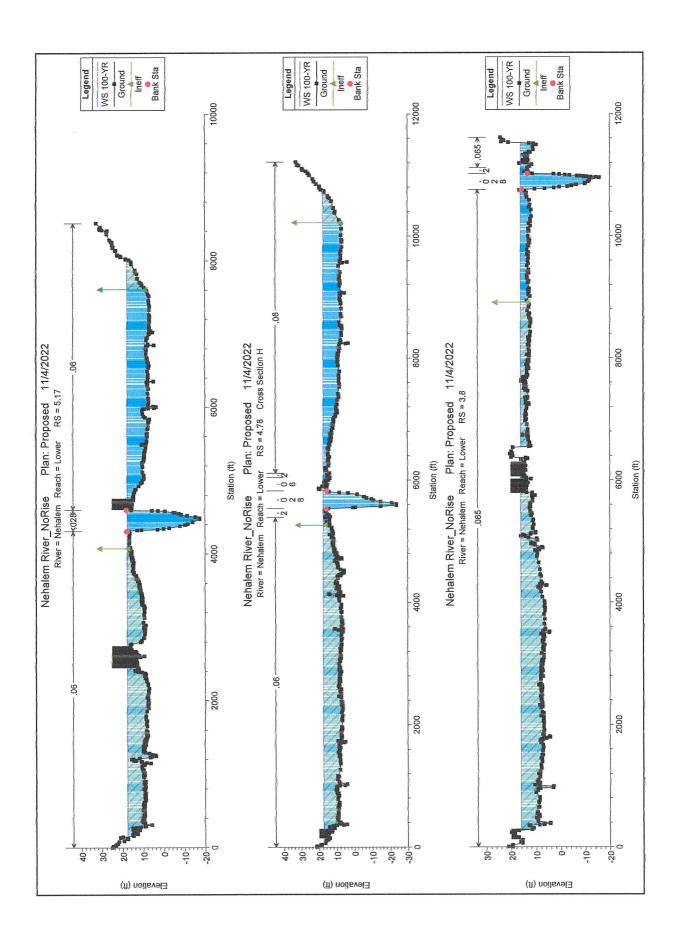


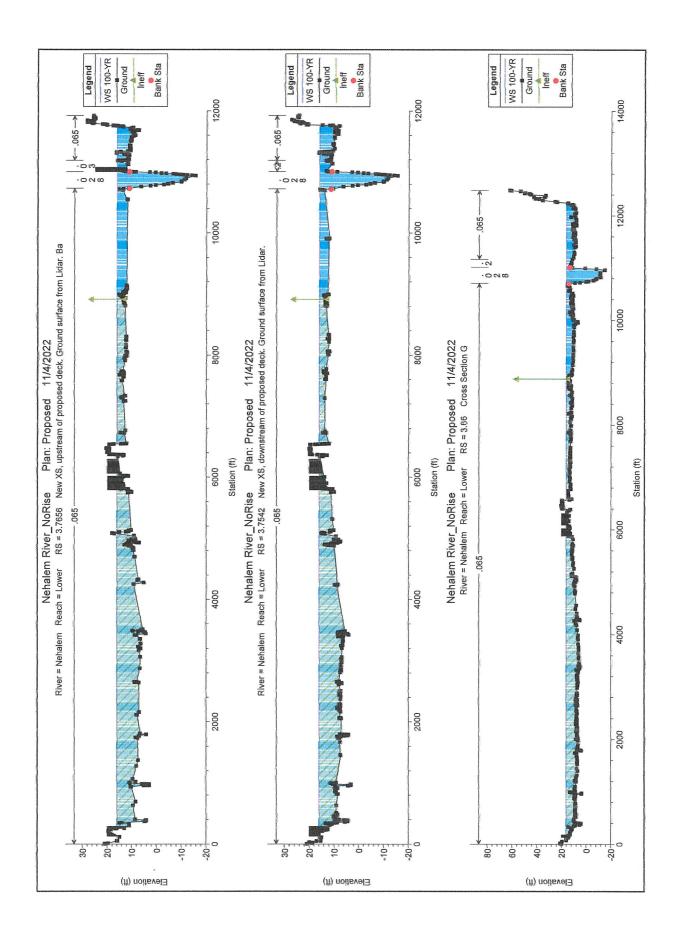


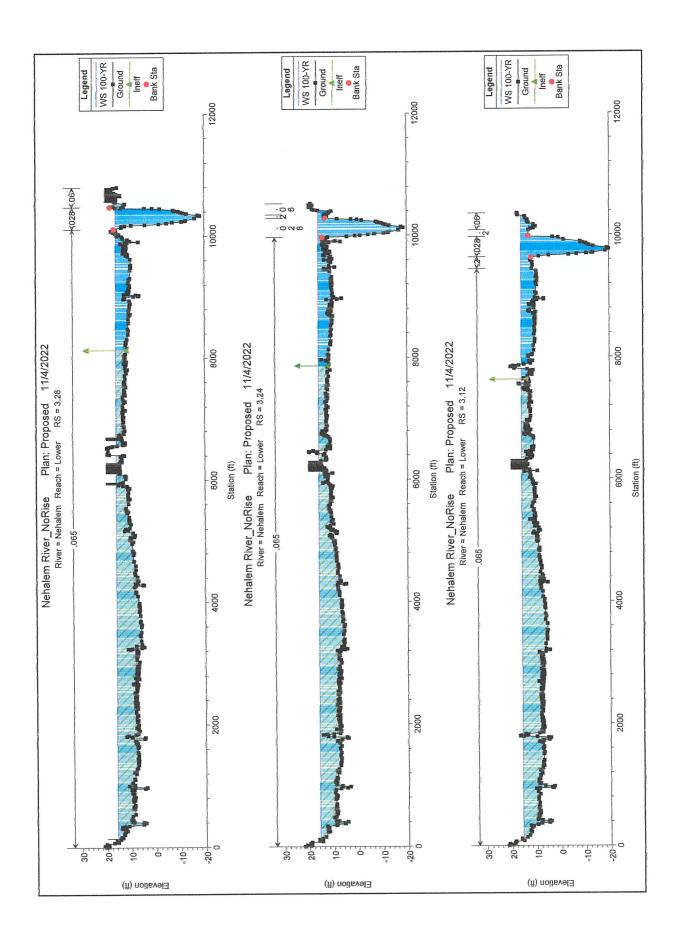


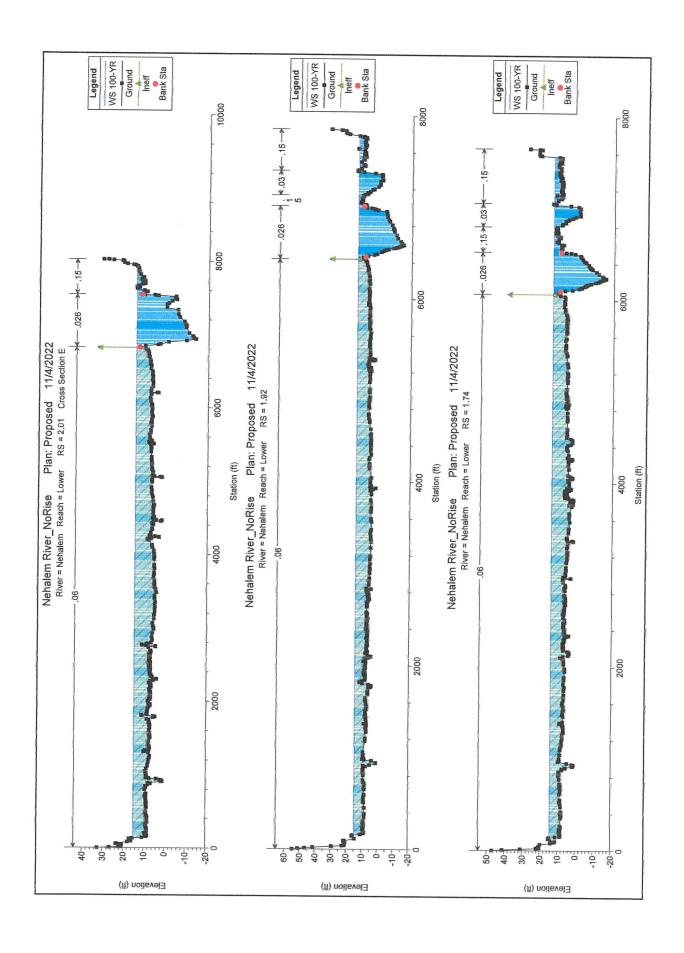


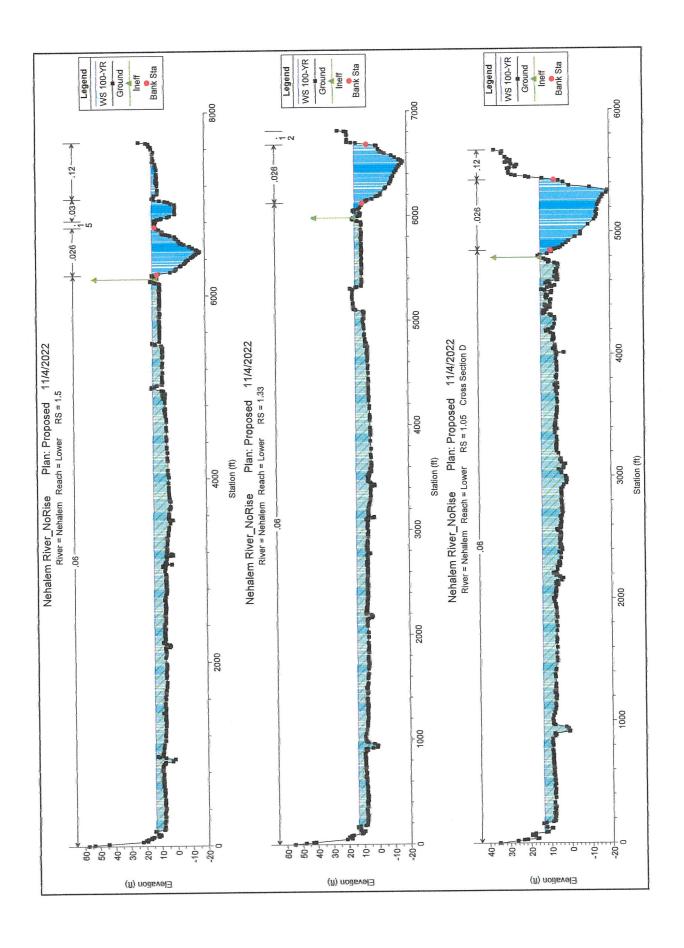


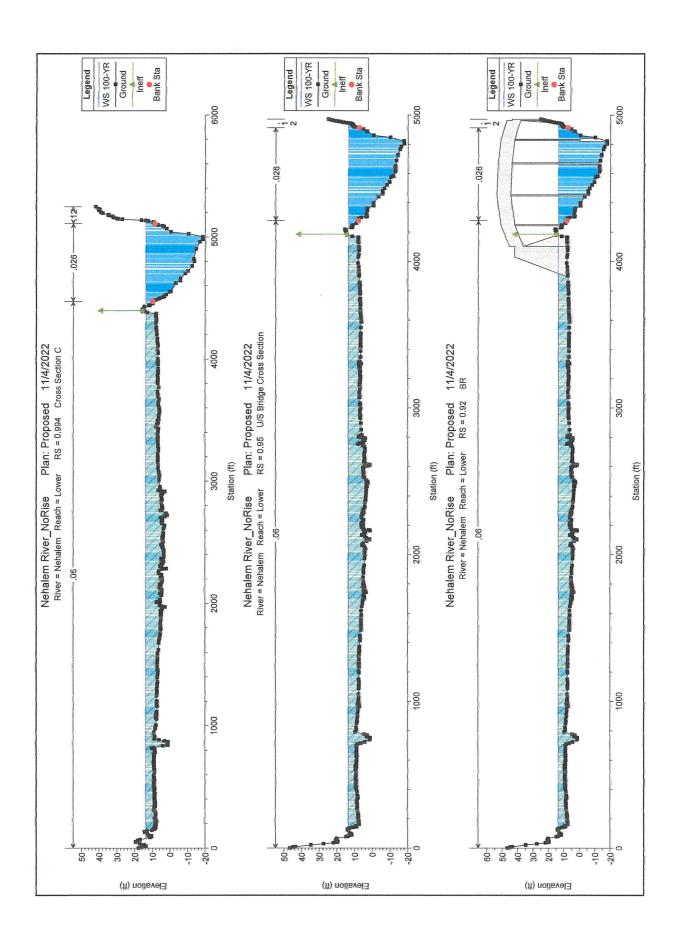


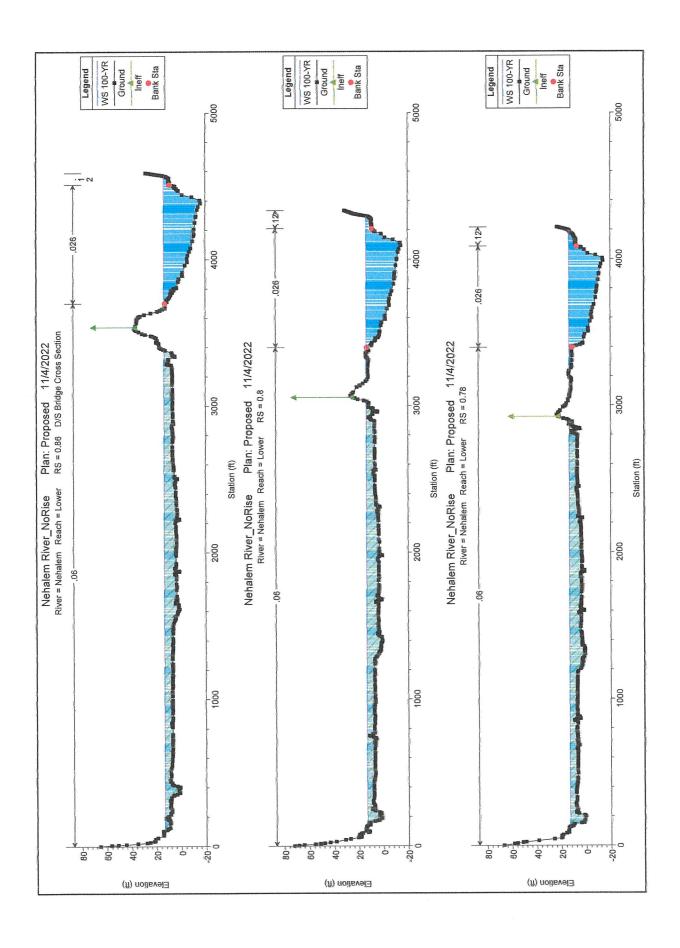


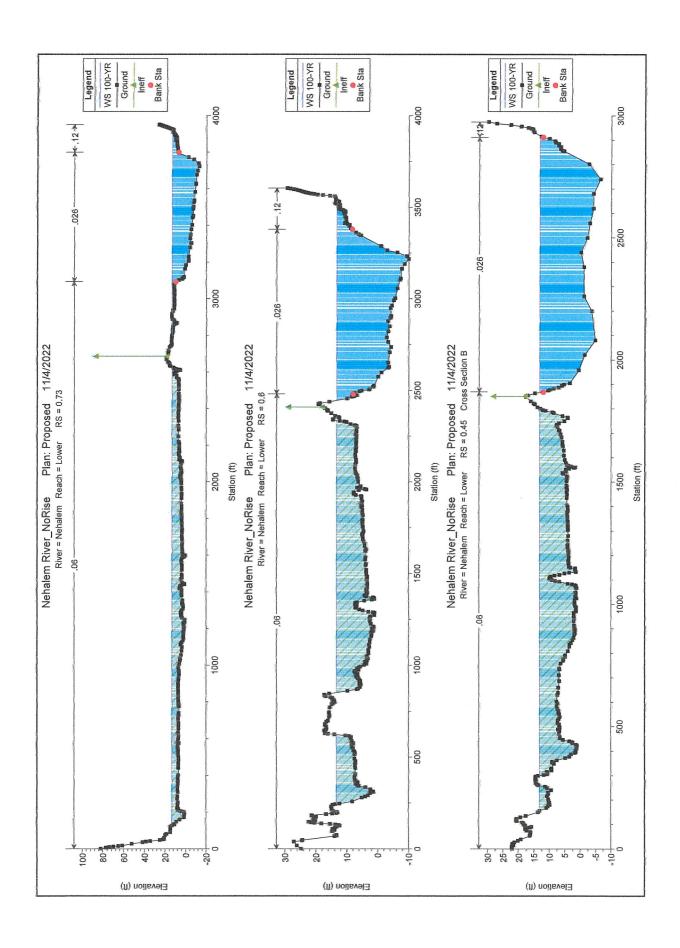


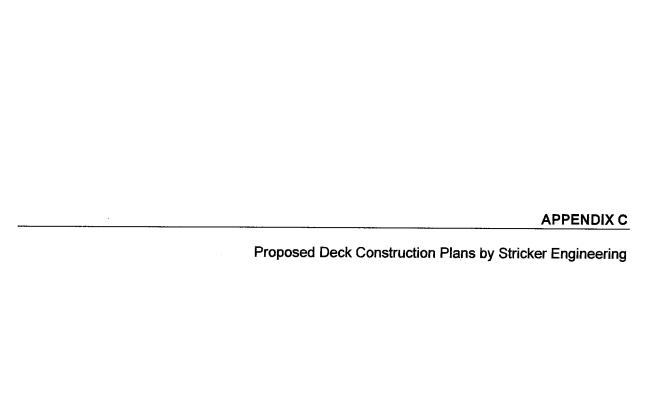












COVER SHEET 80.0 Drawing N.O. NEHALEM, OR 97131 828-2021 824-2021 NWCHS 8A OR QUANODOM SEES! TRENT AND KELLIE DAVIS
HOUSE RENOVATION

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201 East Cypness 51117 HO, 11118 503-522-2442 moo.gnineenignensoring.com





## SHEET INDEX:

NAILING SCHEDULE NOTES

NAILING SCHEDULE

Control and the second of the

WOOD FRAMING

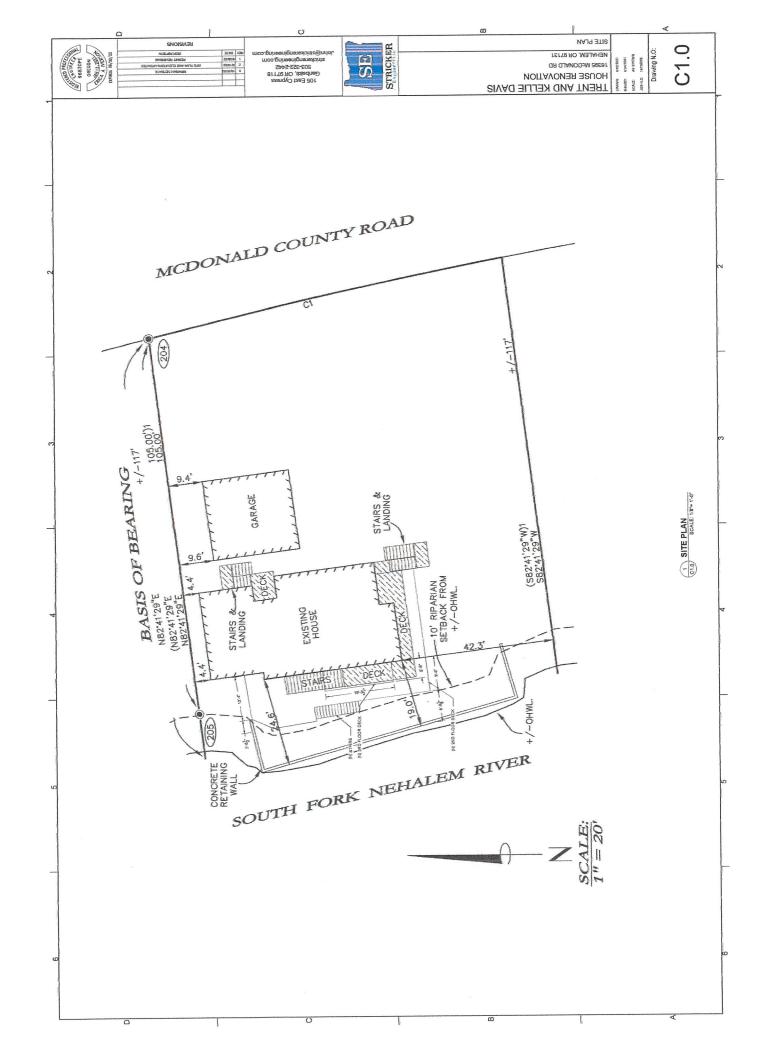
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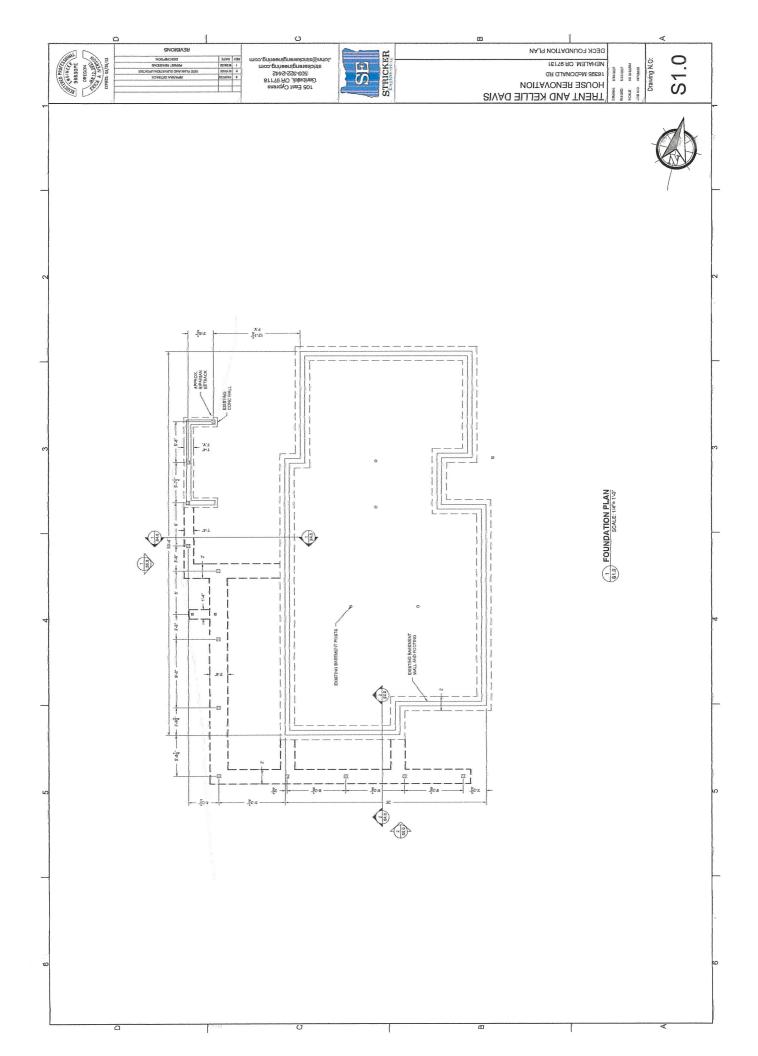
STRUCTURAL DESIGN NOTES

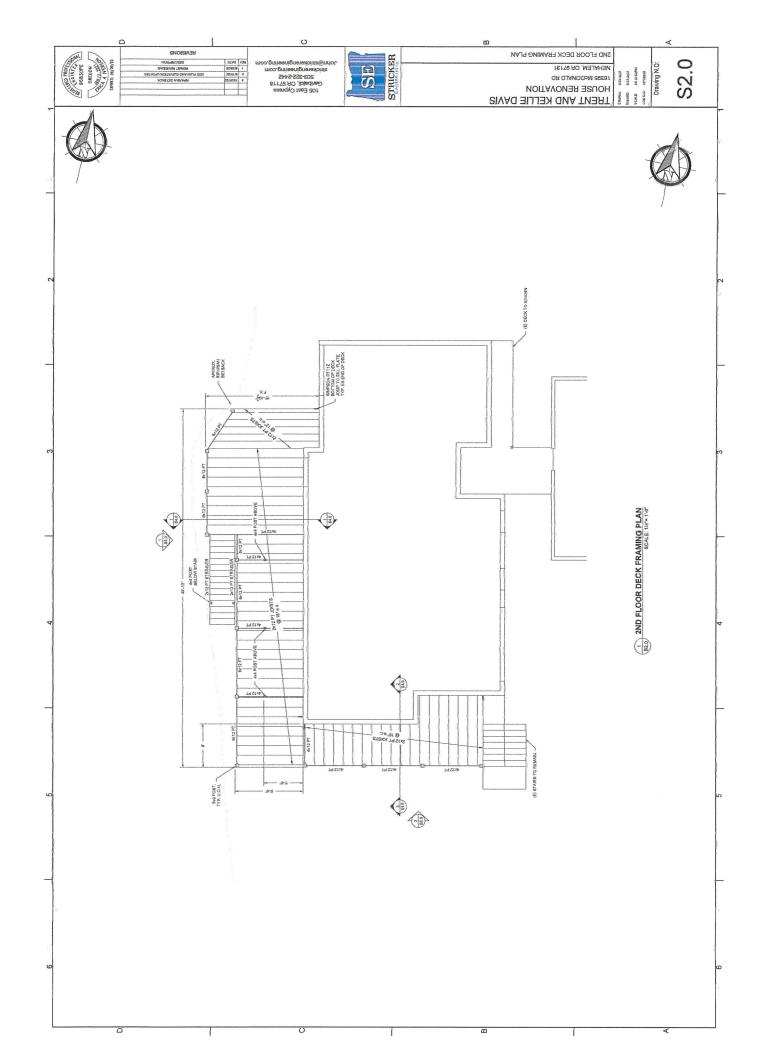
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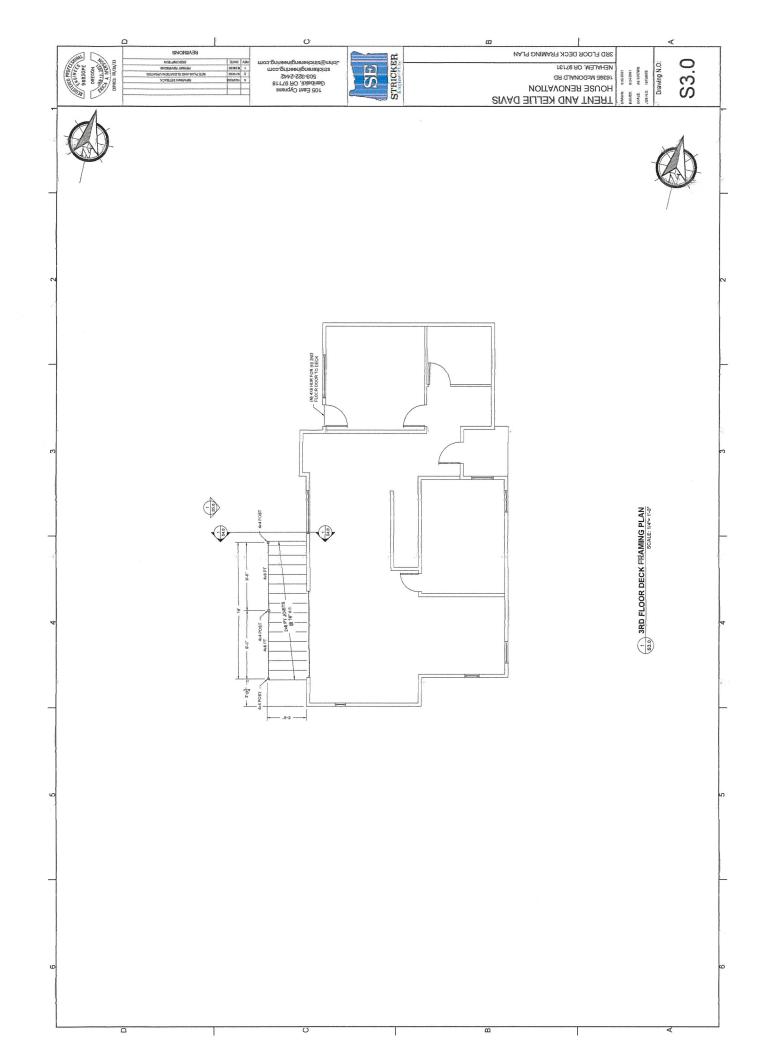
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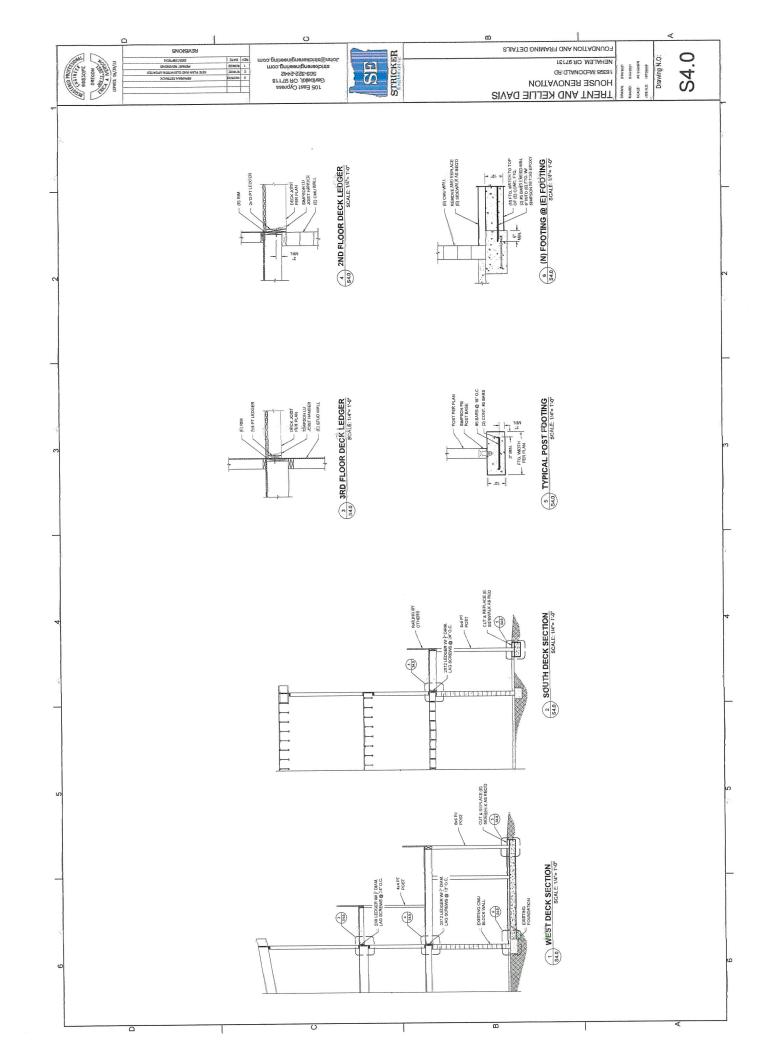
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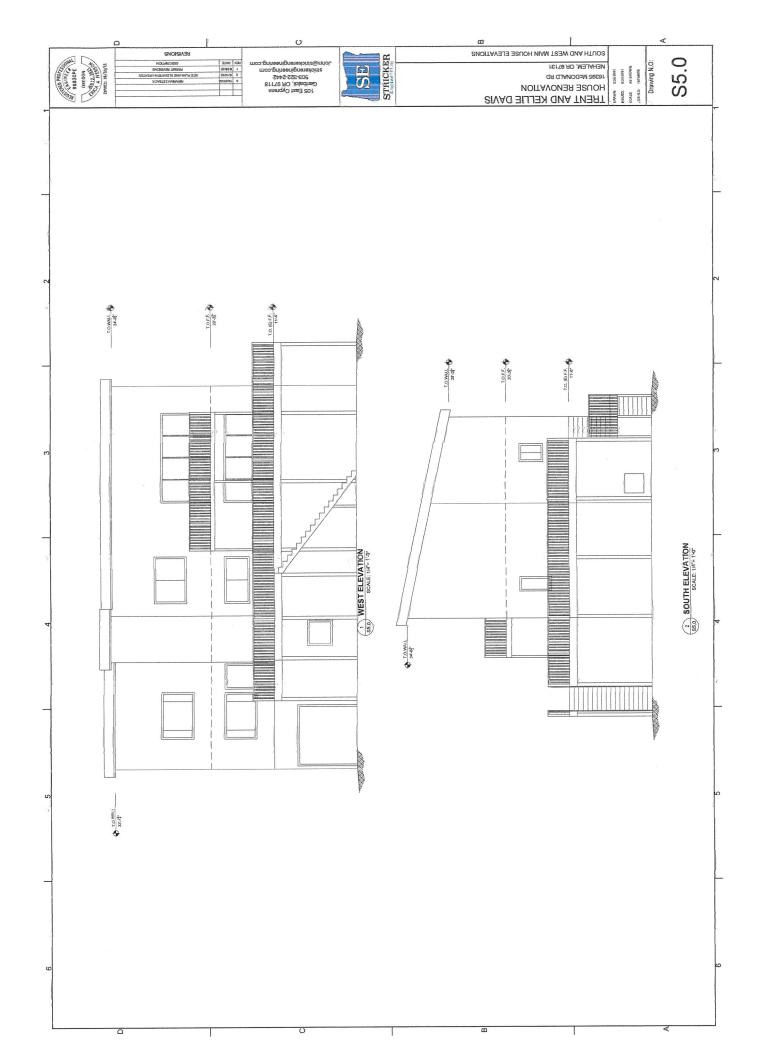












## APPENDIX D

Photo Log

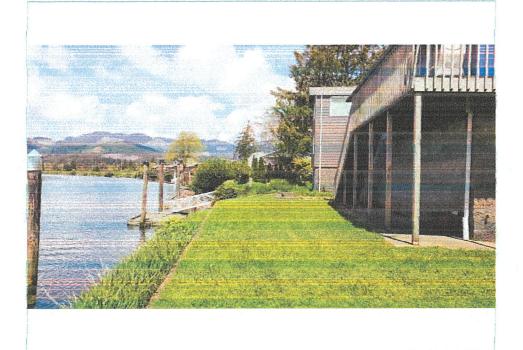


Photo 1: West side of Davis property

Western side of the Davis property, with the Nehalem River on the left, the existing deck and house on the right, and a grass lawn between the two.



Photo 2: Nehalem River -Upstream

Looking upstream at the Nehalem River from the Davis property.



PROCESSED: RS DATE

PROJECT NO.: 1026

Nov 2022

**PAGE** 

APPENDIX D

No-Rise Report Nehalem River at 16395 McDonald Dike Road Nehalem, Oregon

PHOTOGRAPH LOG

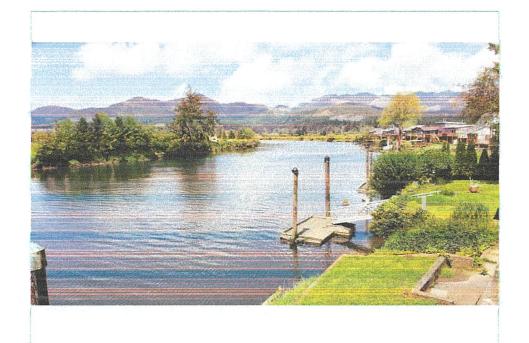


Photo 3: Nehalem River -Downstream

Looking downstream at the Nehalem River from the Davis property.



Cascade Water Resources, LLC

PROJECT NO.: 1026

PROCESSED:

DATE

Nov 2022

RS

PAGE

APPENDIX D

No-Rise Report Nehalem River at 16395 McDonald Dike Road Nehalem, Oregon

PHOTOGRAPH LOG